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# SITE-SPECIFIC TECHNICAL REPORT FOR FREE PRODUCT RECOVERY TESTING AT SITE S-4, BIR 348 KELLY AFB, TEXAS

# **DRAFT**



# PREPARED FOR:

AIR FORCE CENTER FOR ENVIRONMENTAL EXCELLENCE TECHNOLOGY TRANSFER DIVISION (AFCEE/ERT) 8001 ARNOLD DRIVE BROOKS AFB, TEXAS 78235-5357

**AND** 

KELLY AFB, NY TX

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### **DRAFT**

# SITE-SPECIFIC TECHNICAL REPORT (A003)

for

# FREE PRODUCT RECOVERY TESTING AT SITE S-4, KELLY AFB, TEXAS

by

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#### **EXECUTIVE SUMMARY**

This report summarizes the field activities conducted at Kelly Air Force Base (AFB) for a short-term field pilot test to compare vacuum-enhanced free-product recovery (bioslurping) to traditional free-product recovery techniques used to remove light, nonaqueous-phase liquid (LNAPL) from subsurface soils and aquifers. The field testing at Kelly AFB is part of the Bioslurper Initiative, which is funded and managed by the U.S. Air Force Center for Environmental Excellence (AFCEE) Technology Transfer Division. The AFCEE Bioslurper initiative is a multisite program designed to evaluate the efficacy of the bioslurping technology for (1) recovery of LNAPL from groundwater and the capillary fringe, and (2) enhancing natural in situ degradation of petroleum contaminants in the vadose zone via bioventing.

The main objective of the Bioslurper Initiative is to develop procedures for evaluating the potential for recovering free-phase LNAPL present at petroleum-contaminated sites. The overall study is designed to evaluate bioslurping and identify site parameters that are reliable predictors of bioslurping performance. To measure LNAPL recovery in a wide variety of in situ conditions, tests are being performed at many sites. The test at Kelly AFB is one of more than 40 similar field tests to be conducted at various locations throughout the United States and its possessions.

The intent of field testing is to collect data to support determination of the predictability of LNAPL recovery and to evaluate the applicability, cost, and performance of the bioslurping technology for removal of free product and remediation of the contaminated area. The on-site testing is structured to allow direct comparison of the LNAPL recovery achieved by bioslurping with the performance of more conventional LNAPL recovery technologies. The test method included an initial site characterization followed by LNAPL recovery testing. The three LNAPL recovery technologies tested at Kelly AFB were skimmer pumping and bioslurping.

Bioslurper pilot test activities were conducted at two monitoring wells: MW-11 and MW-9. Site characterization activities were conducted to evaluate site variables that could affect LNAPL recovery efficiency and to determine the bioventing potential of the site. Testing included baildown testing to evaluate the mobility of LNAPL, soil gas permeability testing to determine the radius of influence, and in situ respiration testing to evaluate site microbial activity.

Following the site characterization activities, the pump tests were conducted. At monitoring well MW-11, pilot tests for skimmer pumping and bioslurping were conducted. The LNAPL

recovery testing was conducted in the following sequence: 40.9 hr in the skimmer configuration, 117.5 hr in the bioslurper configuration, and an additional 22 hr in the skimmer configuration.

At monitoring well MW-9, pilot tests for bioslurping were conducted. The LNAPL recovery testing was conducted for 23.9 hr in the bioslurper configuration.

Measurements of extracted soil gas composition, LNAPL thickness, and groundwater level were taken throughout the testing. The volume of LNAPL recovered and groundwater extracted were quantified over time.

Baildown recovery tests were conducted at three monitoring wells: MW-8, MW-9, and MW-11. Baildown recovery tests provide a qualitative indication of the presence of mobile, free-phase LNAPL and recovery potential. Overall the baildown recovery tests indicated a relatively rapid rate of LNAPL recovery into the wells. Short-term baildown recovery resulted in LNAPL thicknesses greater than or equal to the initial apparent thicknesses at monitoring wells MW-9 and MW-11. Based on these results, pilot testing was initiated on monitoring well MW-11, with a short-term bioslurper pump test also conducted at monitoring well MW-9.

Skimmer pump testing was conducted at monitoring well MW-11 in a continuous extraction mode for 40.9 hours. Small quantities of free-phase LNAPL were recovered during the two days of skimmer pump testing, indicating that gravity-driven recovery is minimal. Bioslurper testing was conducted for five days with significantly greater recoveries than during skimmer pumping. The recovery rate during the bioslurper pump test was 38 gallons/day during the first day and dropped to 26 gallons/day by day 3; however, the recovery rate increased to 39 gallons/day by day 5. Vacuum levels in the well were relatively low at 22"H<sub>2</sub>O. The second skimmer pump test resulted in significantly greater LNAPL recoveries than observed during the first skimmer pump test, with an average LNAPL recovery rate of 21 gallons/day. These results indicate that the vacuum-enhanced bioslurper mode may have increased the LNAPL mobility, resulting in better recovery during skimmer pumping.

Groundwater production was relatively high during skimmer pumping and bioslurping, with a total of 27,000 gallons of groundwater produced. After the groundwater flowed though a filter tank and oil/water separator, the groundwater was pumped into an industrial waste line connected to the Base Industrial Wastewater Treatment Plant. Contaminant concentrations (3.5 mg TPH/L) were compatible with typical discharge guidelines.

In an effort to determine if the results at monitoring well MW-11 were representative of site conditions, bioslurper testing was conducted at monitoring well MW-9. Similar quantities of free-

phase LNAPL were recovered during this bioslurper pump test, with 49 gallons/day recovered. The wellhead vacuum on monitoring well MW-9 (5"H<sub>2</sub>O) and groundwater production rate (5,300 gallons/day) were similar to those observed at monitoring well MW-11. Results at monitoring wells MW-11 and MW-9 appear to be representative of the site and indicate that vacuum-enhanced liquid recovery techniques are feasible.

Bioslurping also promotes mass removal in the form of in situ biodegradation via bioventing and soil-gas extraction. Vapor phase mass removal is the result of soil-gas extraction as well as volatilization that occurs during the movement of LNAPL free product through the extraction network. Given the measured vapor flowrate (76 scfm) and vapor concentrations, initial hydrocarbon removal rates were approximately 960 lb/day of TPH. Benzene concentrations were below detection limits. Thus, initially, mass removal in the vapor phase is significant. However, this short-term test does not provide a good indication as to whether these rates would be sustained. Higher vapor mass removal rates are more often sustained at those sites where liquid product recovery is sustained.

The internal combustion engine (ICE) used at the site was capable of reducing TPH emissions by 91%. After ICE treatment, the TPH emissions rate was reduced to approximately 86 lb/day. No benzene was detected in the emissions.

The initial soil-gas profiles at the site displayed high total volatile hydrocarbon vapor conditions across the 5.5- to 14-ft below ground surface horizons; however, oxygen concentrations were not significantly reduced except at one monitoring point (1% oxygen at MPB-13.5). Oxygen concentrations at other monitoring points ranged from 10% to 20%. Soil-gas concentrations were measured during the bioslurper test at monitoring points adjacent to monitoring well MW-11 to determine if the vadose zone was being oxygenated via the bioslurper action. Oxygen concentrations were influenced at all monitoring points; however, oxygen concentrations dropped in all cases, so that by the end of the bioslurper pump tests, oxygen concentrations ranged from 1% to 8%. These results indicate that the initial concentrations measured at the monitoring points may have been high due to oxygen diffusion into the soils during monitoring point installation. Once bioslurping was initiated, oxygen-deficient soil gas was pulled past these monitoring points, creating the drop in oxygen concentrations. Based on the soil-gas permeability test, where pressure changes were detected up to 30 ft from the bioslurper well, it is likely that these areas will become fully aerated. In short, a five day extraction time frame at 76 scfm is insufficient to exchange sufficient pore volumes of soil gas to fully oxygenate the zone of influence.

In situ biodegradation rates of 14 to 20 mg/kg-day were measured at three different locations. Based on a radius of influence of 28 ft and a hydrocarbon-impacted soil thickness of 16 ft, mass removal rates via biodegradation are on the order of 48 to 69 lbs of hydrocarbon per day. Thus, mass removal rates via biodegradation could be significant. These results indicate that bioventing is feasible at this site. Air injection bioventing is preferable over bioslurping and soil vapor extraction with respect to the elimination of hydrocarbon vapor emissions.

In summary, the on-site testing at Kelly AFB included the direct testing of gravity-driven and vacuum-driven LNAPL free product recovery techniques, bioventing, physical sampling, and tests relevant to soil vapor extraction. LNAPL recovery was most significant under vacuum-enhanced conditions; therefore, bioslurping is recommended at this site provided long-term treatment of groundwater is economically feasible. Vapor phase mass removal rates measured during bioslurper testing may be the result of soil gas removal (i.e., SVE) or volatilization during liquid entrainment. The generation of off-gas is undesirable and sustained rates of off-gas discharge cannot be estimated accurately from this test. The in situ respiration test and vadose zone radius of influence testing demonstrate that bioventing is feasible at this site.

## DRAFT SITE-SPECIFIC TECHNICAL REPORT (A003)

for

# FREE PRODUCT RECOVERY TESTING AT SITE S-4, KELLY AFB, TEXAS

21 May 1997

#### 1.0 INTRODUCTION

This report describes activities performed and data collected during field tests at Kelly Air Force Base (AFB), Texas to compare vacuum-enhanced free-product recovery (bioslurping) to traditional free-product recovery technologies for removal of light, nonaqueous-phase liquid (LNAPL) from subsurface soils and aquifers. The field testing at Kelly AFB is part of the Bioslurper Initiative, which is funded and managed by the U.S. Air Force Center for Environmental Excellence (AFCEE) Technology Transfer Division. The AFCEE Bioslurper Initiative is a multisite program designed to evaluate the efficacy of the bioslurping technology for (1) recovery of LNAPL from groundwater and the capillary fringe and (2) enhancing natural in situ degradation of petroleum contaminants in the vadose zone via bioventing.

#### 1.1 Objectives

The main objective of the Bioslurper Initiative is to develop procedures for evaluating the potential for recovering free-phase LNAPL present at petroleum-contaminated sites. The overall study is designed to evaluate bioslurping and identify site parameters that are reliable predictors of bioslurping performance. To measure LNAPL recovery in a wide variety of in situ conditions, tests are being performed at many sites. The test at Kelly AFB is one of more than 40 similar field tests to be conducted at various locations throughout the United States and its possessions. Aspects of the testing program that apply to all sites are described in the Test Plan and Technical Protocol for Bioslurping (Battelle, 1995). Test provisions specific to activities at Kelly AFB are described in the Site-Specific Test Plan provided in Appendix A.

The intent of field testing is to collect data to support determination of the predictability of LNAPL recovery and to evaluate the applicability, cost, and performance of the bioslurping

technology for removal of free product and remediation of the contaminated area. The on-site testing is structured to allow direct comparison of the LNAPL recovery achieved by bioslurping with the performance of more conventional LNAPL recovery technologies. The test method included an initial site characterization followed by LNAPL recovery testing. The two LNAPL recovery technologies tested at Kelly AFB were skimmer pumping and bioslurping. The specific test objectives, methods, and results for the Kelly AFB test program are discussed in the following sections.

# 1.2 Testing Approach

Bioslurper pilot test activities were conducted at two monitoring wells: MW-11 and MW-9. Site characterization activities were conducted to evaluate site variables that could affect LNAPL recovery efficiency and to determine the bioventing potential of the site. Testing included baildown testing to evaluate the mobility of LNAPL, soil gas permeability testing to determine the radius of influence, and in situ respiration testing to evaluate site microbial activity.

Following the site characterization activities, the pump tests were conducted. At monitoring well MW-11, pilot tests for skimmer pumping and bioslurping were conducted. The LNAPL recovery testing was conducted in the following sequence: 40.9 hr in the skimmer configuration, 117.5 hr in the bioslurper configuration, and an additional 22 hr in the skimmer configuration.

At monitoring well MW-9, pilot tests for bioslurping were conducted. The LNAPL recovery testing was conducted for 23.9 hr in the bioslurper configuration.

Measurements of extracted soil gas composition, LNAPL thickness, and groundwater level were taken throughout the testing. The volume of LNAPL recovered and groundwater extracted were quantified over time.

#### 2.0 SITE DESCRIPTION

The information presented in the Site Description portion of this Test Plan was obtained from the document titled, Draft Technical Memorandum for the Quintana Road Project Site S-4 (Prepared for the U.S. Air Force Installation Program, Kelly Air Force Base, San Antonio, Texas. Submitted to the HAZWRAP Support Contractor Office, Oak Ridge, Tennessee. General Order Number 188-

97381C, Task Y-03, Volume I of II Text, by NUS, 1990). This document is referenced as NUS 1990 in this Test Plan text.

Site S-4 is located at the southeastern edge of Kelly AFB in Zone 3 and extends off base across Berman Road to the UPR yard and the Quintana Road residential area (Figure 1). Within Site S-4 are active (F/367) and abandoned (F/371) UST facilities and their associated subsurface pipelines. Facility F/371 was constructed in 1943 and contained 5 USTs. These tanks were used to store JP-4 jet fuel but were taken out of service in 1984 and eventually abandoned in 1986. Approximately 2,000 ft of underground piping was removed from operation in 1982 after pressure tests indicated that the system contained extensive leaks (NUS 1990).

Subsurface contamination at Site S-4 was documented during storm drain excavations along Quintana Road by the City of San Antonio in 1985 and 1988. A fuel-like substance was observed floating on exposed groundwater in trenches excavated to a depth of 30 ft below ground surface (bgs). The LNAPL was subsequently identified as JP-4 jet fuel, based on analyses conducted by the Texas Water Commission.

Following the detection of subsurface free product, Radian Corporation conducted site surveys under the Installation Restoration Program (IRP) and subsequent surveys were preformed by NUS Corporation under the Hazardous Waste Remedial Actions Program (HAZWRAP). During these activities, site geological characteristics, groundwater movement, and extent of subsurface contamination were investigated.

#### 2.1 Site Geology

Soil at Site S-4 was found to be heterogeneous in nature, containing nonuniform layers of sand, gravel, silt, and clays. The site was characterized as containing alluvial sediment deposits that reside on the eroded surface of the underlying Navarro clay. Caliche also was identified, occurring either as randomly distributed nodules or as concentrated layers of gravel-sized nodules. This complex geological formation contributes to fluctuating groundwater depths, variable groundwater flow patterns, dry soil areas, and the apparent "pooling" of the subsurface LNAPL contamination.

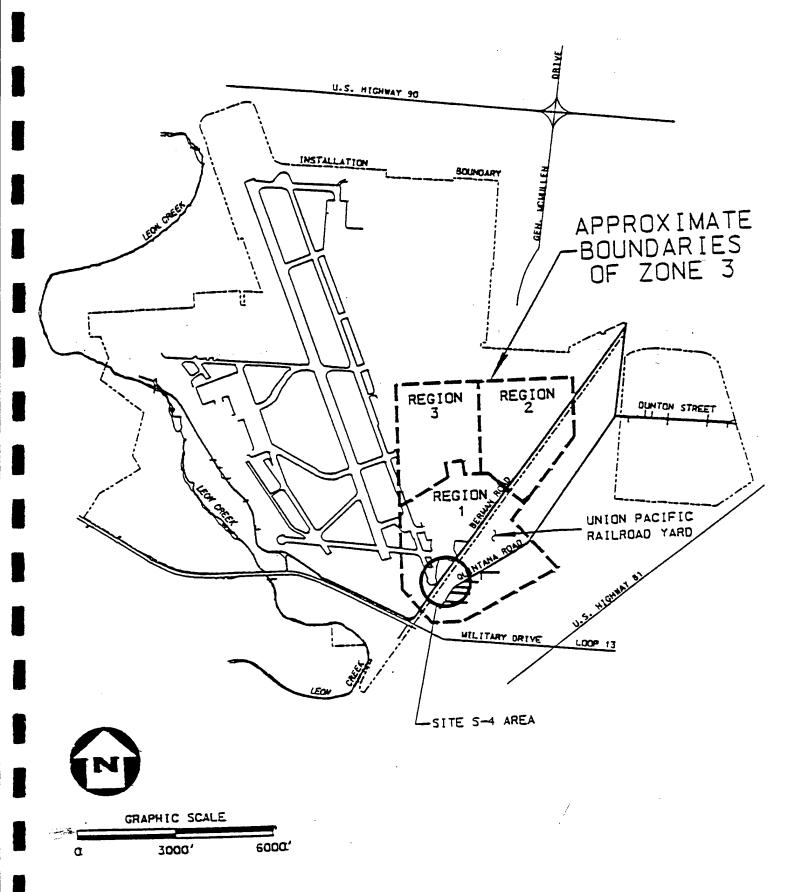


Figure 1. Schematic Diagram Showing Location of Site S-4 at Kelly AFB

#### 2.2 Aguifer Characteristics

Groundwater at Site S-4 occurs at depths ranging from 14 to 16 ft bgs. In characterizing the aquifer, both slug and pump tests have been performed at the site. Results indicate that the average hydraulic conductivity of the aquifer is  $1.87 \times 10^{-2}$  cm/sec, with conductivities ranging from  $1.32 \times 10^{-1}$  cm/sec to  $1.14 \times 10^{-4}$  cm/sec (NUS 1990). The average transmissivity across the pump test area was calculated to be 158.2 ft<sup>2</sup>/day (NUS 1990).

The Basewide Hydrogeologic Assessment (BHA) performed by NUS in 1990 indicates that the groundwater gradient at Site S-4 generally slopes to the south-southwest. Measurements from the site surveys confirm this, but the gradient is not uniform. At the center of Site S-4, the gradient decreases markedly from 0.0042 ft/ft north of Z307 to 0.0014 ft/ft between Z307 and Z301 (NUS 1990). The gradient is relatively flat in the north-south direction between wells Z337 and UP05, but it steepens again south of Z317. Also noted in the NUS 1990 report was the identification of a south-southwest depression, or "channel," in the water table that crosses Site S-4.

An elevated occurrence of the Navarro clay has resulted in a dry area at Site S-4. This area affects the groundwater flow by diverting it from a southerly flow to a southwesterly direction. The groundwater gradient and the Navarro-related dry zone have been noted for playing a critical role in shaping the resulting JP-4 plume.

#### 2.3 Site Contamination

Benzene, toluene, ethylbenzene, and xylenes (BTEX) have been identified in the capillary fringe at Site S-4 at concentrations of 407 mg/kg with an average concentration of 100 mg/kg. In the area of UST F/371, soil gas measurements for total volatile hydrocarbons are reported as high as 64,000 ppmv with total BTEX levels of 543 ppmv.

Within the JP-4 plume, three pools of free product have been identified. These pools are centered around wells S405, Z301/Z302/Z303, and Z313/Z314. During manual bailing, well Z302 along with UP03 and Z313, consistently produced more than 3 gallons of product per half hour of continuous bailing. The field test of the bioslurper technology will likely intercept one of these 3 identified pools of free product at Site S-4. The preferred area is that associated with wells Z301/Z302/Z303 at the UPR yard off the southeastern edge of Kelly AFB (Figure 2).

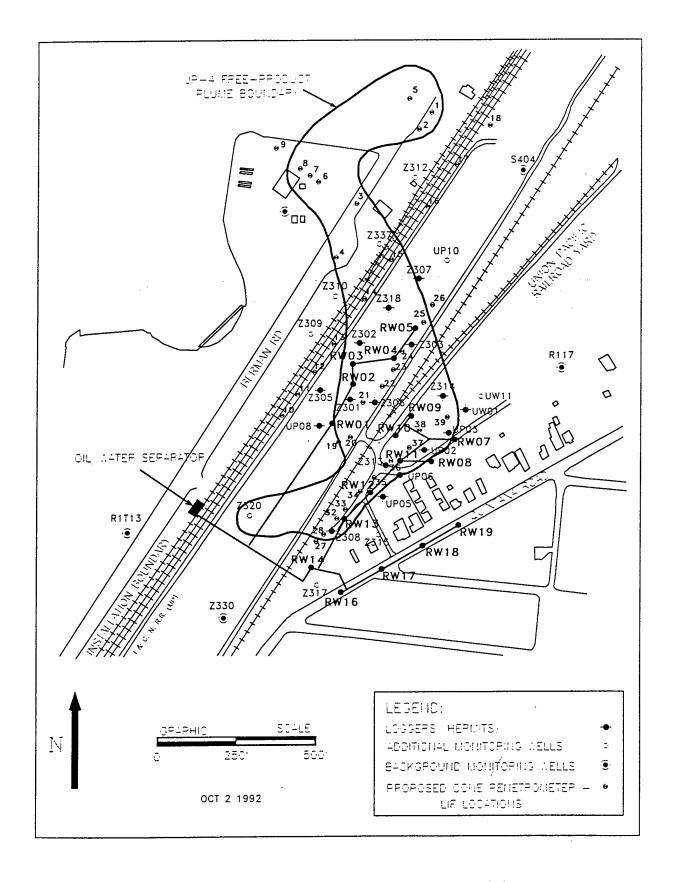


Figure 2. Location of Recovery Wells Within Site S-4

Estimates of total LNAPL contamination at Site S-4 have also been made. Based upon measured fuel thickness and the areal extent of subsurface contamination, the estimated volume of JP-4 present in the formation across the plume area ranges from 150,000 to 240,000 gallons (SAALC, 1994). Only a portion of the total volume will be impacted during the bioslurper test.

#### 3.0 FREE-PRODUCT RECOVERY PILOT TEST METHODS

This section documents the initial conditions at the test site and describes the test equipment and methods used for the short-term pilot test at Kelly AFB. Soil samples were not collected because the sampling equipment available could not penetrate to the capillary fringe.

#### 3.1 Initial LNAPL/Groundwater Measurements and Baildown Testing

Monitoring wells MW-8, MW-9, and MW-11 were evaluated for use in the bioslurper pilot testing. Initial depths to LNAPL and to groundwater were measured using an oil/water interface probe (ORS Model #1068013). LNAPL was removed from the well with a Teflon® bailer until the LNAPL thickness could no longer be reduced. A total of 2.825 L (0.75 gallons), 6.7 L (1.8 gallons), and 7.38 L (1.9 gallons) of free-phase LNAPL was removed from monitoring wells MW-8, MW-9, and MW-11, respectively, at the start of the baildown tests. The rate of increase in the thickness of the floating LNAPL layer was monitored using the oil/water interface probe for approximately 16 hr at each monitoring well.

#### 3.2 Well Construction Details

Short-term pump tests were conducted at monitoring wells MW-11 and MW-9. Precise construction details for these monitoring wells has not yet been received from the Base. A schematic diagram illustrating general well construction details for monitoring well MW-11 is provided in Figure 3.

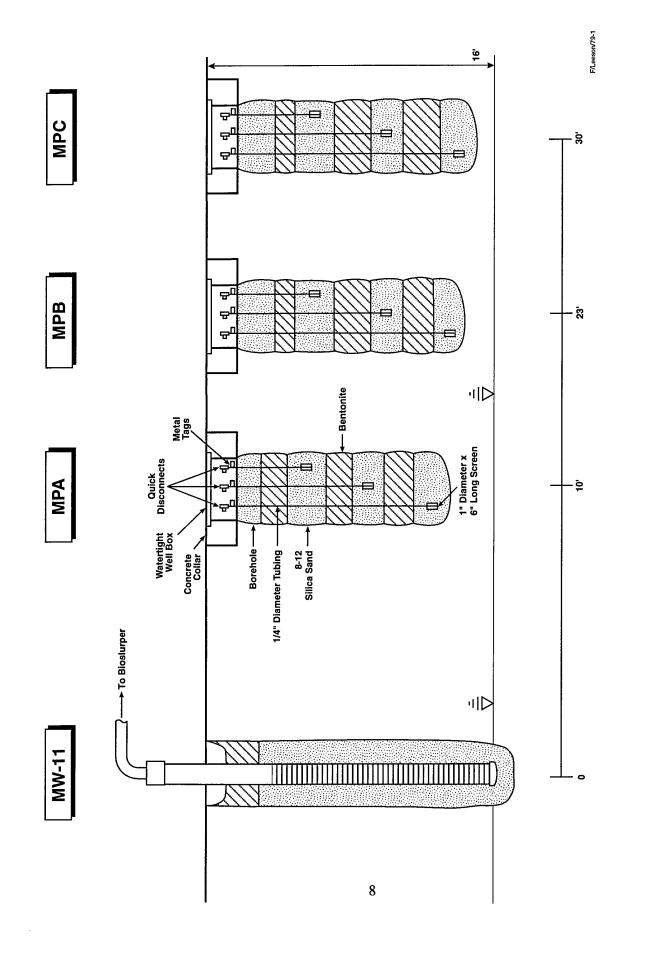


Figure 3. Schematic Diagram Showing Construction Details of Monitoring Well MW-11 and Soil Gas Monitoring Points

#### 3.3 Soil Gas Monitoring Point Installation

Three monitoring points were installed and labeled MPA, MPB, and MPC. The locations and general constructions details of the monitoring points are illustrated in Figure 3.

Monitoring points consisted of ¼-inch tubing, with 1-inch-diameter, 6-inch-long screened areas. The annular space corresponding to the screened length was filled with silica sand. The interval from the top of the screened length to the bottom of the next screened length, as well as the interval from the ground surface to the top of the first screened length, was filled with bentonite clay chips. After placement, the bentonite clay was hydrated with water to expand the chips and provide a seal. At monitoring point MPA, the ends of the screened lengths were positioned at depths of 5.5, 9.0, and 12.5 ft bgl. At monitoring point MPB, the ends of the screened lengths were positioned at depths of 6.0, 10, and 13.5 ft bgl. At monitoring point MPC, the screened lengths were positioned at depths of 6.0, 10, and 14 ft bgl.

After installation of the monitoring points, initial soil gas measurements were taken with a GasTech portable  $O_2/CO_2$  meter and a GasTech TraceTechtor portable hydrocarbon meter. Oxygen concentrations were relatively high at all monitoring points, although TPH concentrations also were high (Table 1), indicating that microbial activity may be fairly low or that oxygen levels could be elevated from installation activities. Results from the in situ respiration test will provide more information concerning microbial activity.

## 3.4 LNAPL Recovery Testing

3.4.1 System Setup

-A100 is a 7.5 Hp

The bioslurping pilot test system is a trailer-mounted mobile unit. The vacuum pump (Atlantic Fluidics Model A100, 10-hp liquid ring pump), filter box, oil/water separator, and required support equipment were carried to the test location on a trailer. The trailer was located near the monitoring well, the well cap was removed, a well seal was placed on the top of the well, and the drop tube was lowered into the well. The drop tube was attached to the vacuum pump. Different configurations of the well seal and the placement depth of the drop tube allow for simulation of skimmer pumping, operation in the bioslurping configuration, or simulation of drawdown pumping. Extracted soil gas was treated through an internal combustion engine (ICE). Data from the ICE is

**Table 1. Initial Soil-Gas Compositions** 

Monitoring Point	Depth (ft)	Oxygen (%)	Carbon Dioxide (%)	TPH (ppmv)
MPA	5.5	20.0	0.25	4,200
	9.0	19.5	0.25	9,200
	12.5	11.0	7.0	>20,000
MPB	MPB 6.0		NM	NM
	10	16.0	0.5	>20,000
	13.5	1.0	1.0	>20,000
MPC	6.0	15.0	0.5	>20,000
	10	16.0	0.5	>20,000
	14	10.0	1.0	>20,000

provided in Appendix B. Extracted groundwater was treated by passing the recovered fluid through the filter box, the oil/water separator, and a 325-gallon settling tank. The treated groundwater was then discharged to the Base Industrial Wastewater Treatment Plant.

A brief system startup test was performed prior to LNAPL recovery testing to ensure that all system components were working properly. The system checklist is provided in Appendix C. All site data and field testing information were recorded in a field notebook and then transcribed onto pilot test data sheets provided in Appendix D.

#### 3.4.2 Skimmer Pump Test

Prior to test initiation, depths to LNAPL and groundwater were measured. The liquid ring pump was used to conduct the skimmer pump test with the wellhead open to the atmosphere (Figure 4). The drop tube was held in position at 16.6 ft below the top of the well casing. The pump was started 1430, 11 November 1996, to begin the skimmer pump test. The test was operated for a total of 40.9 hr. The pump vacuum was approximately 22"Hg and the vapor flowrate from the well was approximately 100 scfm. The LNAPL and groundwater extraction rates were monitored throughout

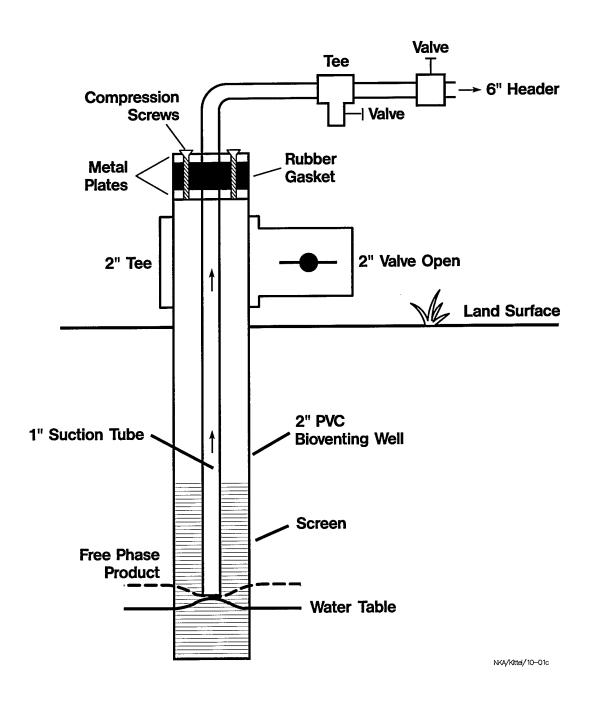


Figure 4. Drop Tube Placement and Valve Position for the Skimmer Pump Test

the test, as were all other relevant data for the skimmer pump test. Test data sheets are provided in Appendix D.

# 3.4.3 Bioslurper Pump Test

## 3.4.3.1 Monitoring Well MW-11

Upon completion of the skimmer pump test, preparations were made to begin the bioslurper pump test at monitoring well MW-11. The LNAPL and groundwater depth were measured prior to any recovery testing. The slurper tube was set at the LNAPL/groundwater interface at a depth of approximately 15.7 ft bgl. The sanitary well seal was positioned inside the well, sealing the wellhead and allowing the pump to establish a vacuum in the well (Figure 5). A pressure gauge was installed at the wellhead to measure the vacuum inside the extraction well. The liquid ring pump was started at 1119, 14 November 1996, to begin the bioslurper pump test. The test was initiated approximately 4 hr after the skimmer pump test and was operated for 117.5 hr. The pump vacuum was approximately 26"Hg, the vapor flowrate from the well was approximately 72 scfm, and the well vacuum was approximately 19"H<sub>2</sub>O, and the drop tube vacuum was approximately 19"Hg. The LNAPL and groundwater extraction rates were monitored throughout the test, as were all other relevant data for the bioslurper pump test. The data sheets are provided in Appendix D.

An LNAPL sample was collected at 1300, 17 November 1997, from the oil/water separator during the bioslurper pump test and was labeled K-LNAPL-1. The sample was sent to Alpha Analytical, Inc., in Sparks, Nevada for analysis of BTEX.

## 3.4.3.2 Monitoring Well MW-9

Upon completion of the bioslurper pump test at monitoring well MW-11, preparations were made to begin the bioslurper pump test at monitoring well MW-9. The LNAPL and groundwater depth were measured prior to any recovery testing. The drop tube was set at the LNAPL/groundwater interface at a depth of 17.8 ft below top of well casing. The sanitary well seal was positioned inside the well, sealing the wellhead and allowing the pump to establish a vacuum in the well. A pressure gauge was installed at the wellhead to measure the vacuum inside the extraction well. The liquid ring pump was started at 1308, 19 November 1996, to begin the bioslurper pump

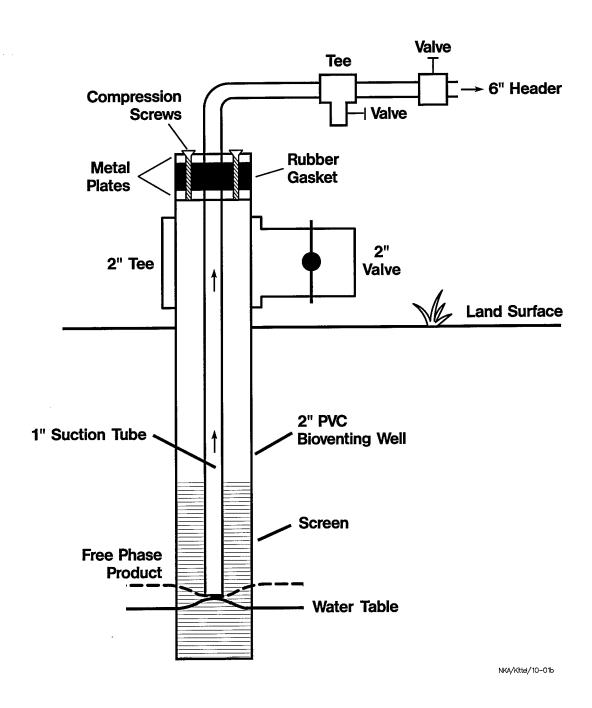


Figure 5. Drop Tube Placement and Valve Position for the Bioslurper Pump Test

test. The test was initiated approximately 3 hr after the MW-11 bioslurper pump test and was operated for 23.9 hr. The pump vacuum was approximately 25.5"Hg, the vapor flowrate was approximately 82 scfm, the well vacuum was approximately 5"H<sub>2</sub>O, and the drop tube vacuum was approximately 19"Hg. The LNAPL and groundwater extraction rates were monitored throughout the test, as were all other relevant data for the bioslurper pump test. The data sheets are provided in Appendix D.

#### 3.4.4 Second Skimmer Pump Test

Upon completion of the bioslurper pump test at monitoring well MW-9, preparations were made to begin the second skimmer pump test at monitoring well MW-11. Prior to test initiation, depths to LNAPL and groundwater were measured. The liquid ring pump was used to conduct the skimmer pump test with the wellhead open to the atmosphere. The drop tube was held in position at 16.5 ft below the top of the well casing. The pump was started 1445, 20 November 1996, to begin the second skimmer pump test. The test was operated for a total of 22 hr. The pump vacuum was approximately 25.5"Hg and the vapor flowrate from the well was approximately 83 scfm. The LNAPL and groundwater extraction rates were monitored throughout the test, as were all other relevant data for the skimmer pump test. Test data sheets are provided in Appendix D.

#### 3.4.5 Off-Gas Sampling and Analysis

Five off-gas samples were collected during the bioslurper pump test at monitoring well MW-11. Samples KLRPV-1 and KLRPV-2 were collected from the seal tank headspace after approximately 71.5 and 102 hr of operation, respectively. Samples KICEV-1 and KICEV-2 were collected from the ICE off-gas after approximately 72 and 102 hr of operation, respectively. Sample KICEV-SP-1 was collected from the ICE sampling port after approximately 102 hr of operation. The samples were collected in Summa® canisters and sent under chain of custody to Air Toxics, Ltd., in Folsom, California, for analyses of TPH and volatile organic compounds (VOCs), using EPA Method TO-14. Analytical reports are provided in Appendix E.

#### 3.4.6 Groundwater Sampling and Analysis

One groundwater sample was collected during the bioslurper pump test at monitoring well MW-11 and was labeled K-W-1. The sample was collected from the outlet to the industrial treatment plant after 76.5 hr of operation. The sample was collected in a 40-mL VOA vial containing hydrochloric acid (HCl) preservative. The sample was checked to ensure no headspace was present and was then shipped on ice and sent under chain of custody to Alpha Analytical, Inc., in Sparks, Nevada for analyses of BTEX and TPH (purgeable). Analytical reports are provided in Appendix E.

#### 3.5 Bioventing Analyses

## 3.5.1 Soil Gas Permeability Testing

The soil gas permeability test data were collected during the bioslurper pump test at monitoring well MW-11. Before a vacuum was established in the extraction well, the initial soil gas pressures at the three installed monitoring points were recorded. The start of the bioslurper pump test created a steep pressure drop in the extraction well which was the starting point for the soil gas permeability testing. Soil gas pressures were measured at each of the three monitoring points at all depths to track the rate of outward propagation of the pressure drop in the extraction well. Soil gas pressure data were collected frequently during the first 20 minutes of the test. The soil gas pressures were recorded throughout the bioslurper pump test to determine the bioventing radius of influence. Test data are provided in Appendix F.

### 3.5.2 In Situ Respiration Testing

Air was injected into three monitoring points for approximately 24 hr beginning on 20 November 1996. Helium was not used due to a malfunction with equipment. The setup for the in situ respiration test is described in the Test Plan and Technical Protocol a Field Treatability Test for Bioventing (Hinchee et al., 1992). A ½-hp diaphragm pump was used for air injection. Air was injected through monitoring points MPA-12.5, MPB-13.5, and MPC-14.0. After the air/helium injection was terminated, soil gas concentrations of oxygen, carbon dioxide, and TPH were monitored periodically. The in situ respiration test was terminated on 22 November 1996. Oxygen utilization

and biodegradation rates were calculated as described in Hinchee et al. (1992). Raw data for these tests are presented in Appendix G.

#### 4.0 FREE-PRODUCT RECOVERY PILOT TEST RESULTS

This section documents the results of the site characterization, the comparative LNAPL recovery pump test, and other supporting tests conducted at Kelly AFB.

#### 4.1 Baildown Test Results

Results from the baildown tests are presented in Tables 2 through 4. Baildown recovery tests provide a qualitative indication of the presence of mobile, free-phase LNAPL and recovery potential. Overall, the baildown recovery tests indicated a relatively rapid rate of LNAPL recovery into the wells, with monitoring wells MW-9 and MW-11 recovering to initial levels by the end of the 16-hr baildown tests. Based on these results, pilot testing was initiated on monitoring wells MW-11 and MW-9.

#### 4.2 LNAPL Pump Test Results

#### 4.2.1 Initial Skimmer Pump Test Results

Only small quantities of free-phase LNAPL were recovered during the two days of skimmer pump testing, with no measurable LNAPL recovered on day 1 and 8.9 gallons/day on day 2 (Figure 6). A total of 6.3 gallons of LNAPL was recovered (Table 5). Due to the low volume recovered, the LNAPL could not be quantified until the final day of testing. Large volumes of groundwater were produced, averaging 1,500 gallons/day. There results indicate that gravity-driven recovery is minimal.

Table 2. Results of Baildown Testing in Monitoring Well MW-8

Sample Collection Time	Depth to Groundwater (ft)	Depth to LNAPL (ft)	LNAPL Thickness (ft)
Initial Reading 11/11/96-1432	16.45	15.55	0.90
11/11/96-1545	15.83	15.76	0.07
11/11/96-1545.5	15.83	15.74	0.09
11/11/96-1546	15.83	15.74	0.09
11/11/96-1546.5	15.84	15.74	0.10
11/11/96-1547	15.84	15.74	0.10
11/11/96-1548	15.85	15.74	0.11
11/11/96-1549	15.85	15.74	0.11
11/11/96-1550	15.85	15.75	0.10
11/11/96-1555	15.88	15.74	0.14
11/11/96-1615	15.92	15.73	0.19
11/11/96-1655	15.97	15.73	0.24
11/11/96-1726	15.97	15.73	0.24
11/12/96-0751	16.37	15.62	0.75

Table 3. Results of Baildown Testing in Monitoring Well MW-9

Sample Collection Time	Depth to Groundwater (ft)	Depth to LNAPL (ft)	LNAPL Thickness (ft)
Initial Reading 11/11/96-1640	18.29	16.92	1.37
11/11/96-1648	17.28	17.20	0.08
11/11/96-1648.5	17.30	17.20	0.10
11/11/96-1649	17.33	17.20	0.13
11/11/96-1649.5	17.33	17.20	0.13
11/11/96-1650	17.34	17.20	0.14
11/11/96-1650.5	17.34	17.20	0.14
11/11/96-1651	17.35	17.20	0.15
11/11/96-1651.5	17.36	17.20	0.16
11/11/96-1652	17.37	17.20	0.17
11/11/96-1652.5	17.37	17.20	0.17
11/11/96-1658	17.43	17.19	0.24
11/11/96-1703	17.47	17.17	0.30
11/11/96-1713	17.54	17.16	0.38
11/11/96-1743	17.67	17.13	0.54
11/11/96-1813	17.78	17.08	0.70
11/12/96-0750	18.37	16.93	1.44

Table 4. Results of Baildown Testing at Monitoring Well MW-11

Sample Collection Time	Depth to Groundwater (ft)	Depth to LNAPL (ft)	LNAPL Thickness (ft)
Initial Reading 11/11/96-1432	16.59	15.2132.84	1.38
11/11/96-1504	15.57	15.53	0.04
11/11/96-1504.5	15.61	15.52	0.09
11/11/96-1505	15.64	15.51	0.13
11/11/96-1505.5	15.65	15.50	0.15
11/11/96-1506	15.68	15.49	0.19
11/11/96-1506.5	15.69	15.48	0.21
11/11/96-1507	15.72	15.47	0.25
11/11/96-1507.5	15.73	15.47	0.26
11/11/96-1508	15.75	15.47	0.28
11/11/96-1509	15.78	15.47	0.31
11/11/96-1510	15.79	15.47	0.32
11/11/96-1511	15.80	15.47	0.33
11/11/96-1512	15.81	15.47	0.34
11/11/96-1513	15.83	15.46	0.37
11/11/96-1514	15.83	15.46	0.37
11/11/96-1519	15.85	15.45	0.40
11/11/96-1524	15.88	15.44	0.44
11/11/96-1534	15.92	15.43	0.49
11/11/96-1606	16.05	15.43	0.62
11/11/96-1636	16.13	15.38	0.75
11/11/96-1730	16.28	15.35	0.93
11/11/96-1800	16.33	15.33	1.00
11/12/96-0753	16.63	15.25	1.38

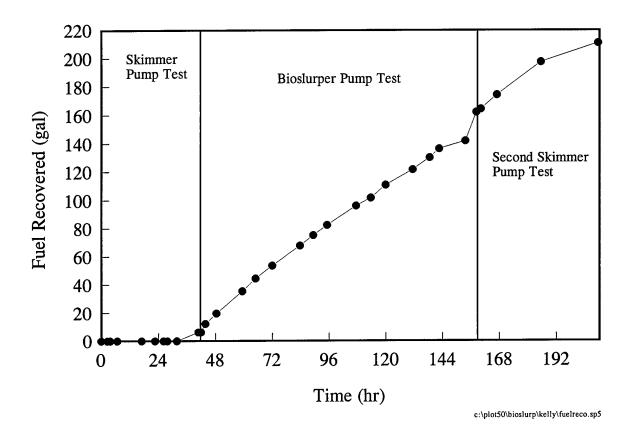


Figure 6. LNAPL Recovery Versus Time During Each Pump Test at Monitoring Well MW-11

Table 5. Pump Test Results at Monitoring Well MW-11

	Recovery Rate (gallons/day)					
Time (Days)	Skimmer Pump Test		Bioslurper Pump Test		Second Skimmer Pump Test	
	LNAPL	Groundwater	LNAPL	Groundwater	LNAPL	Groundwater
1	0	810	38	6,700	21	3,300
2	8.9	2,200	30	5,200	NA	NA
3	NA	NA	26	5,200	NA	NA
4	NA	NA	27	5,300	NA	NA
5	NA	NA	39	5,200	NA	NA
Average	4.5	1,400	32	5,500	21	3,300
Total Recovery (gal)	6.3	2449.6	156	26,784	19.3	3,052

NA = Not applicable.

## 4.2.2 Bioslurper Pump Test Results

### 4.2.2.1 Monitoring Well MW-11

Relatively high volumes of LNAPL was recovered during the bioslurper pump test (Table 5) (Figure 6). Bioslurper testing was conducted for approximately five days, with the LNAPL recovery rate remaining relatively constant throughout testing, with an average recovery rate of 32 gallons/day (Figure 7). A total of 156 gallons of LNAPL and 26,784 gallons of groundwater was extracted.

Soil-gas concentrations were measured during the bioslurper test at monitoring points adjacent to monitoring well MW-11 to determine if the vadose zone was being oxygenated via the bioslurper action. Oxygen concentrations were influenced at all monitoring points; however, oxygen concentrations dropped in all cases, so that by the end of the bioslurper pump tests, oxygen concentrations ranged from 1% to 8% (Table 6). These results indicate that the initial concentrations measured at the monitoring points may have been high due to oxygen diffusion into the soils during monitoring point installation. Once bioslurping was initiated, oxygen-deficient soil gas was pulled

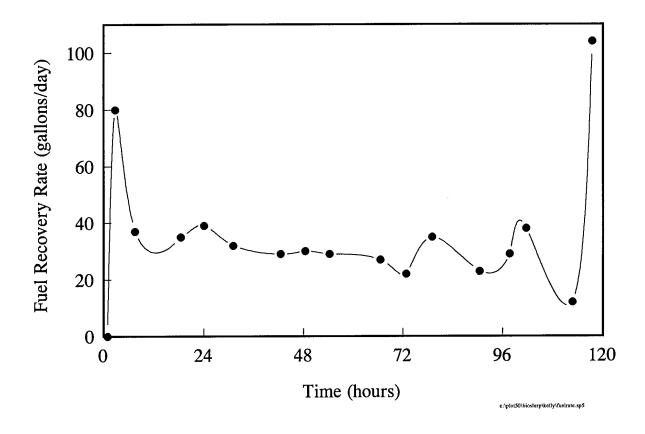


Figure 7. LNAPL Recovery Rate Versus Time During the Bioslurper Pump Test at Monitoring Well MW-11

Table 6. In Situ Soil Gas Oxygen Concentrations During the Bioslurper Pump Test at Monitoring Well MW-11

	Oxygen Concentrations (%) Versus Time (hours)						
Monitoring Point	0	35.7	47.6	56.4	71.3	81.0	97.0
MPA-5.5	20.0	15.0	13.0	10.0	8.0	2.0	2.0
MPA-9.0	19.5	14.5	0.75	14.5	9.5	10.5	8.0
MPA-12.5	11.0	1.0	0.5	10.5	1.5	1.5	1.0
MPB-6.0	NA	NA	NA	NA	NA	NA	NA
MPB-10.0	16.0	1.0	0.25	1.5	1.5	2.0	2.0
MPB-13.5	1.0	0.5	0.25	1.0	1.0	2.0	1.0
MPC-6.0	15.0	13.0	4.5	2.5	9.5	8.5	7.0
MPC-10.0	16.0	15.0	5.0	1.5	10.0	1.5	1.0
MPC-14.0	10.0	5.5	4.5	2.0	1.0	1.5	1.0

past these monitoring points, creating the drop in oxygen concentrations. Based on the soil-gas permeability test, where pressure changes were detected up to 30 ft from the bioslurper well, it is likely that these areas will become fully aerated. In short, a five day extraction time frame at 76 scfm is insufficient to exchange sufficient pore volumes of soil gas to fully oxygenate the zone of influence.

### 4.2.2.2 Monitoring Well MW-9

In an effort to determine if the results at monitoring well MW-11 were representative of site conditions, bioslurper testing was conducted at monitoring well MW-9. As at monitoring well MW-11, the LNAPL recovery rate (49 gallons/day) and groundwater production rate (5,400 gallons/day) were similar to those observed at monitoring well MW-11 (Table 7). The wellhead vacuum on monitoring well MW-9 (5"H<sub>2</sub>O) was somewhat lower than that at monitoring well MW-11. Results at monitoring wells MW-11 and MW-9 appear to be representative of the site and indicate that vacuum-enhanced liquid recovery is feasible.

Table 7. Bioslurper Pump Test Results at Monitoring Well MW-9

	Recovery Rate (gallons/day)				
Time (days)	LNAPL	Groundwater			
1	49	5,400			
Average	49	5,400			
Total Recovery (gallons)	49	5,342			

### 4.2.3 Second Skimmer Pump Test

A second skimmer pump test was conducted to determine if results from the initial skimmer pump test were representative of gravity-driven recovery. LNAPL recovery rates were significantly higher than the initial pump test, with an average recovery of 21 gallons/day. Groundwater production also increased to an average of 3,300 gallons/day. This increase in fluid recovery could be due to enhanced mobility due to the bioslurper.

#### 4.2.4 Extracted Groundwater, LNAPL, and Off-Gas Analyses

Results of the groundwater analyses are shown in Table 8. Contaminant concentrations were relatively low, with TPH concentrations 3.5 mg/L and all BTEX compounds below detection limits. The on-site water treatment equipment, consisting of a filter tank, oil/water separator, and clarification tanks, resulted in water effluent that is considered compatible with typical sanitary sewer discharge limits.

The results from the off-gas analyses are presented in Table 9. BTEX compounds were below detection limits, while small amounts of chlorinated compounds were detected, although these were removed by the ICE. Given a vapor flowrate from the well of 76 scfm and an average TPH concentration of 22,000 ppmv before treatment, initial hydrocarbon removal rates were approximately 960 lb/day of TPH. Thus, initially, mass removal in the vapor phase is significant. However, this short-term test does not provide a good indication of whether these rates would be sustained. Higher vapor mass removal rates are more often sustained at those sites where liquid product recovery is

Table 8. BTEX and TPH Concentrations in Extracted Groundwater During the Bioslurper Pump Test at Monitoring Well MW-11

Parameter	K-W-1
TPH (purgeable)	3.5
Benzene	< 0.0020
Toluene	< 0.0020
Ethylbenzene	< 0.0020
Total Xylenes	< 0.0020

NA = Not applicable.

Table 9. Contaminant Concentrations in Off-Gas During the Bioslurper Pump Test at Monitoring Well MW-11

	Concentration (ppmv)				
Parameter	KLRPV-1 KICEV-1 KLRPV-2 KICEV-2 KICE-SP-1				
TPH as jet fuel	15,000	760	29,000	1,600	770
Benzene	< 0.40	< 0.071	< 0.71	< 0.092	< 0.087
Toluene	< 0.40	< 0.071	< 0.71	< 0.092	< 0.087
Ethylbenzene	< 0.40	< 0.071	< 0.71	< 0.092	< 0.087
Total Xylenes	< 0.40	< 0.071	< 0.71	< 0.092	0.10
cis-1,2-Dichloroethene	2.6	< 0.071	2.9	< 0.092	< 0.087
Trichloroethene	3.2	< 0.071	2.7	< 0.092	< 0.087
1,2,4-Trimethylbenzene	3.0	0.13	5.4	0.34	0.35
Cyclohexane	3.2	< 0.28	3.9	< 0.37	< 0.35
Heptane	<1.6	< 0.28	2.9	< 0.37	< 0.35

sustained. After ICE treatment, at a vapor flowrate of 127 scfm and using an average TPH concentration of 1,180 ppmv, approximately 86 lb/day TPH was emitted during the bioslurper pump test. These results demonstrated the treatment efficiency of the ICE, with 91% destruction of TPH.

The composition of LNAPL is shown in Table 10 in terms of BTEX concentrations.

Table 10. BTEX Concentrations in LNAPL

Compound	Concentration (mg/kg)
Benzene	< 500
Toluene	< 500
Ethylbenzene	< 500
Total Xylenes	< 500

# 4.3 Bioventing Analyses

# 4.3.1 Soil Gas Permeability and Radius of Influence

The radius of influence is calculated by plotting the log of the pressure change at a specific monitoring point versus the distance from the extraction well. The radius of influence is then defined as the distance from the extraction well where 0.10 inch of  $H_2O$  can be measured. Based on this definition, a radius of influence of 28 ft was determined (Figure 9).

# 4.3.2 In Situ Respiration Test Results

Results from the in situ respiration test are presented in Table 11. Oxygen utilization rates were relatively high, ranging from 0.83 to 1.1 %O<sub>2</sub>/hr. Biodegradation rates ranged from 14 to 18 mg/kg-day. These results indicate that biodegradation in these locations is significant and that bioventing is feasible at this site.

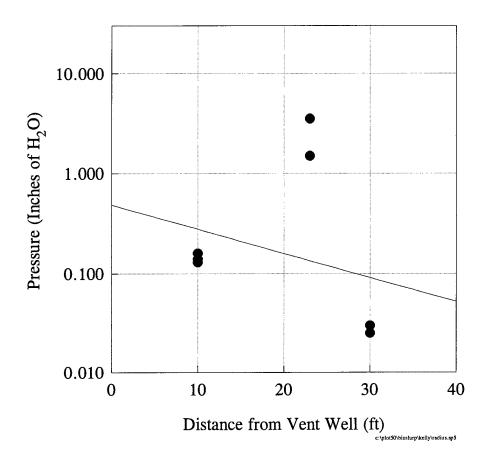


Figure 8. Radius of Influence Determination Using Soil Gas Pressure Change Versus Distance From Extraction Well

Table 11. In Situ Respiration Test Results

Monitoring Point	Oxygen Utilization Rate (%/day)	Biodegradation Rate (mg/kg-day)
MPA-12.5	0.83	14
MPB-13.5	1.1	18
MPC-14.0	0.98	16

#### 5.0 DISCUSSION AND CONCLUSIONS

The main objectives of the field pilot test at Kelly AFB were to determine if LNAPL recovery is feasible and to select the most effective method of LNAPL recovery.

Baildown recovery tests were conducted at three monitoring wells: MW-8, MW-9, and MW-11. Baildown recovery tests provide a qualitative indication of the presence of mobile, free-phase LNAPL and recovery potential. Overall the baildown recovery tests indicated a relatively rapid rate of LNAPL recovery into the wells. Short-term baildown recovery resulted in LNAPL thicknesses greater than or equal to the initial apparent thicknesses at monitoring wells MW-9 and MW-11. Based on these results, pilot testing was initiated on monitoring well MW-11, with a short-term bioslurper pump test also conducted at monitoring well MW-9.

Skimmer pump testing was conducted at monitoring well MW-11 in a continuous extraction mode for 40.9 hours. Small quantities of free-phase LNAPL were recovered during the two days of skimmer pump testing, indicating that gravity-driven recovery is minimal. Bioslurper testing was conducted for five days with significantly greater recoveries than during skimmer pumping. The recovery rate during the bioslurper pump test was 38 gallons/day during the first day and dropped to 26 gallons/day by day 3; however, the recovery rate increased to 39 gallons/day by day 5. Vacuum levels in the well were relatively low at 22"H<sub>2</sub>O. The second skimmer pump test resulted in significantly greater LNAPL recoveries than observed during the first skimmer pump test, with an average LNAPL recovery rate of 21 gallons/day. These results indicate that the vacuum-enhanced bioslurper mode may have increased the LNAPL mobility, resulting in better recovery during skimmer pumping.

Groundwater production was relatively high during skimmer pumping and bioslurping, with a total of 27,000 gallons of groundwater produced. After the groundwater flowed though a filter tank and oil/water separator, the groundwater was pumped into an industrial waste line connected to the Base Industrial Wastewater Treatment Plant. Contaminant concentrations (3.5 mg TPH/L) were compatible with typical discharge guidelines.

In an effort to determine if the results at monitoring well MW-11 were representative of site conditions, bioslurper testing was conducted at monitoring well MW-9. Similar quantities of free-phase LNAPL were recovered during this bioslurper pump test, with 49 gallons/day recovered. The wellhead vacuum on monitoring well MW-9 (5"H<sub>2</sub>O) and groundwater production rate (5,300 gallons/day) were similar to those observed at monitoring well MW-11. Results at monitoring wells MW-11 and MW-9 appear to be representative of the site and indicate that vacuum-enhanced liquid recovery techniques are feasible.

Bioslurping also promotes mass removal in the form of in situ biodegradation via bioventing and soil-gas extraction. Vapor phase mass removal is the result of soil-gas extraction as well as volatilization that occurs during the movement of LNAPL free product through the extraction network. Given the measured vapor flowrate (76 scfm) and vapor concentrations, initial hydrocarbon removal rates were approximately 960 lb/day of TPH. Benzene concentrations were below detection limits. Thus, initially, mass removal in the vapor phase is significant. However, this short-term test does not provide a good indication as to whether these rates would be sustained. Higher vapor mass removal rates are more often sustained at those sites where liquid product recovery is sustained.

The ICE used at the site was capable of reducing TPH emissions by 91%. After ICE treatment, the TPH emissions rate was reduced to approximately 86 lb/day. No benzene was detected in the emissions.

The initial soil-gas profiles at the site displayed high total volatile hydrocarbon vapor conditions across the 5.5- to 14-ft below ground surface horizons; however, oxygen concentrations were not significantly reduced except at one monitoring point (1% oxygen at MPB-13.5'). Oxygen concentrations at other monitoring points ranged from 10% to 20%. Soil-gas concentrations were measured during the bioslurper test at monitoring points adjacent to monitoring well MW-11 to determine if the vadose zone was being oxygenated via the bioslurper action. Oxygen concentrations were influenced at all monitoring points; however, oxygen concentrations dropped in all cases, so that by the end of the bioslurper pump tests, oxygen concentrations ranged from 1% to 8%. These results indicate that the initial concentrations measured at the monitoring points may have been high due to

oxygen diffusion into the soils during monitoring point installation. Once bioslurping was initiated, oxygen-deficient soil gas was pulled past these monitoring points, creating the drop in oxygen concentrations. Based on the soil-gas permeability test, where pressure changes were detected up to 30 ft from the bioslurper well, it is likely that these areas will become fully aerated. In short, a five day extraction time frame at 76 scfm is insufficient to exchange sufficient pore volumes of soil gas to fully oxygenate the zone of influence.

In situ biodegradation rates of 14 to 20 mg/kg-day were measured at three different locations. Based on a radius of influence of 28 ft and a hydrocarbon-impacted soil thickness of 16 ft, mass removal rates via biodegradation are on the order of 48 to 69 lbs of hydrocarbon per day. Thus, mass removal rates via biodegradation could be significant. These results indicate that bioventing is feasible at this site. Air injection bioventing is preferable over bioslurping and soil vapor extraction with respect to the elimination of hydrocarbon vapor emissions.

In summary, the on-site testing at Kelly AFB included the direct testing of gravity-driven and vacuum-driven LNAPL free product recovery techniques, bioventing, physical sampling, and tests relevant to soil vapor extraction. LNAPL recovery was most significant under vacuum-enhanced conditions; therefore, bioslurping is recommended at this site provided long-term treatment of groundwater is economically feasible. Vapor phase mass removal rates measured during bioslurper testing may be the result of soil gas removal (i.e., SVE) or volatilization during liquid entrainment. The generation of off-gas is undesirable and sustained rates of off-gas discharge cannot be estimated accurately from this test. The in situ respiration test and vadose zone radius of influence testing demonstrate that bioventing is feasible at this site.

#### 6.0 REFERENCES

Battelle, 1995. Test Plan and Technical Protocol for Bioslurping. Report prepared by Battelle Columbus Operations for the U.S. Air Force Center for Environmental Excellence, Brooks Air Force Base, Texas.

Hinchee, R.E., S.K. Ong, R.N. Miller, D.C. Downey, and R. Frandt. 1992. Test Plan and Technical Protocol for a Field Treatability Test for Bioventing (Rev. 2). Report prepared by Battelle Columbus Operations, U.S. Air Force Center for Environmental Excellence, and Engineering Sciences, Inc., for the U.S. Air Force Center for Environmental Excellence, Brooks Air Force Base, Texas.

# APPENDIX A

SITE-SPECIFIC TEST PLAN FOR BIOSLURPER FIELD ACTIVITIES AT KELLY AFB, TEXAS

# SITE-SPECIFIC TEST PLAN FOR BIOSLURPER TESTING AT KELLY AIR FORCE BASE, TEXAS (A002) CONTRACT NO. F41624-94-C-8012

**FINAL** 

to

U.S. Air Force Center for Environmental Excellence
Technology Transfer Division
(AFCEE/ERT)
8001 Arnold Drive
Building 642
Brooks AFB, TX 78235

for

Kelly AFB SA-ALC/EMR

June 6, 1995

by

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# SITE-SPECIFIC TEST PLAN FOR BIOSLURPER FIELD ACTIVITIES AT KELLY AIR FORCE BASE, TEXAS

#### **FINAL**

U.S. Air Force Center for Environmental Excellence
Technology Transfer Division
(AFCEE/ERT)
Brooks AFB, TX

June 6, 1995

#### 1.0 INTRODUCTION

The Air Force Center for Environmental Excellence (AFCEE) Technology Transfer Division is conducting a nationwide application of an innovative technology for free-product recovery and soil bioremediation. The technology tested in the Bioslurper Initiative is vacuum-enhanced free-product recovery/bioremediation (bioslurping). The field test and evaluation are intended to demonstrate the initial feasibility of bioslurping by measuring system performance in the field. The Bioslurper Initiative has been designed to evaluate the effectiveness of bioslurping as a light, nonaqueous-phase liquid (LNAPL) recovery technology relative to conventional gravity-driven LNAPL recovery technologies. System performance parameters, mainly free-product recovery, will be determined at numerous sites. Field testing will be performed at many sites to determine the effects of different organic contaminant types and concentrations and different geological conditions on bioslurping effectiveness.

Plans for the field test activities are presented in two documents. The first is the overall Test Plan and Technical Protocol for the entire program, titled *Test Plan and Technical Protocol for Bioslurping* (Battelle, 1995). The overall Test Plan and Technical Protocol is supplemented by plans specific to each test site. The concise site-specific plans communicate vapor and aqueous discharge rates for complying with regulatory requirements specific for the base to base personnel.

The overall Test Plan and Technical Protocol was developed as a generic plan for the Bioslurper Initiative to improve the accuracy and efficiency of Test Plan preparation and ensure consistent data collection across all test sites. The field program requires installation and operation of the bioslurping system supported by a wide variety of site characterization, performance monitoring, and chemical analysis activities. The basic methods to be applied from site to site do not change. Preparation and review of the overall Test Plan and Technical Protocol allows efficient documentation and review of the basic approach to the test program. Peer and regulatory review were performed for the overall Test Plan and Technical Protocol to ensure the credibility of the overall program.

This letter report is the site-specific Test Plan for the field testing approach at Kelly Air Force Base (AFB), Texas. It was prepared based on site-specific information received by Battelle from Kelly AFB and other pertinent site-specific information to support the generic Test Plan and Technical Protocol.

Site-specific information for Kelly AFB identifies at least three areas at Site S-4 within Zone 3 where JP-4 free product exists. Maximum product thickness was measured at monitoring well Z302 beneath the Union Pacific Railroad (UPR) yard off the southeastern edge of Kelly AFB. This area is considered to

be the most likely candidate for the bioslurper field test, with one of the existing recovery wells (RW02, RW03, or RW04) expected to be used. If this area is found to be unsuitable, then alternative sites include the area around monitoring well S405, which is up gradient of the underground storage tank (UST) area F/367, and the area northwest of Quintana Road in the vicinity of monitoring wells Z313 and Z314, using an existing recovery well (RW09, RW10, or RW11).

In order to supplement existing site characterization data and bioslurper application, the AFCEE/ERT will mobilize a cone penetrometer equipped with a laser-induced fluorescence sensor (CPT-LIF). The CPT-LIF will provide continuous lithological and laser induced fluorescence profiling. The laser-induced fluorescence sensor provides useful information on fuel contaminant distribution based on the characteristic fluorescence response of polycyclic aromatic fuel constituents (i.e., napthalenes).

# 2.0 SITE DESCRIPTION

The information presented in the Site Description portion of this Test Plan was obtained from the document titled, *Draft Technical Memorandum for the Quintana Road Project Site S-4* (Prepared for the U.S. Air Force Installation Program, Kelly Air Force Base, San Antonio, Texas. Submitted to the HAZWRAP Support Contractor Office, Oak Ridge, Tennessee. General Order Number 188-97381C, Task Y-03, Volume I of II Text, by NUS, 1990). This document is referenced as NUS 1990 in this Test Plan text.

Site S-4 is located at the southeastern edge of Kelly AFB in Zone 3 and extends off base across Berman Road to the UPR yard and the Quintana Road residential area (Figure 1). Within Site S-4 are active (F/367) and abandoned (F/371) UST facilities and their associated subsurface pipelines. Facility F/371 was constructed in 1943 and contained 5 USTs. These tanks were used to store JP-4 jet fuel but were taken out of service in 1984 and eventually abandoned in 1986. Approximately 2,000 ft of underground piping was removed from operation in 1982 after pressure tests indicated that the system contained extensive leaks (NUS 1990).

Subsurface contamination at Site S-4 was documented during storm drain excavations along Quintana Road by the City of San Antonio in 1985 and 1988. A fuel-like substance was observed floating on exposed groundwater in trenches excavated to a depth of 30 ft below ground surface (bgs). The LNAPL was subsequently identified as JP-4 jet fuel, based on analyses conducted by the Texas Water Commission.

Following the detection of subsurface free product, Radian Corporation conducted site surveys under the Installation Restoration Program (IRP) and subsequent surveys were preformed by NUS Corporation under the Hazardous Waste Remedial Actions Program (HAZWRAP). During these activities, site geological characteristics, groundwater movement, and extent of subsurface contamination were investigated.

# 2.1 Site Geology

Soil at Site S-4 was found to be heterogeneous in nature, containing nonuniform layers of sand, gravel, silt, and clays. Cross-sectional profiles of the area were generated and are presented in Appendix A along with additional geotechnical data. The site was characterized as containing alluvial sediment deposits that reside on the eroded surface of the underlying Navarro clay. Caliche also was identified,

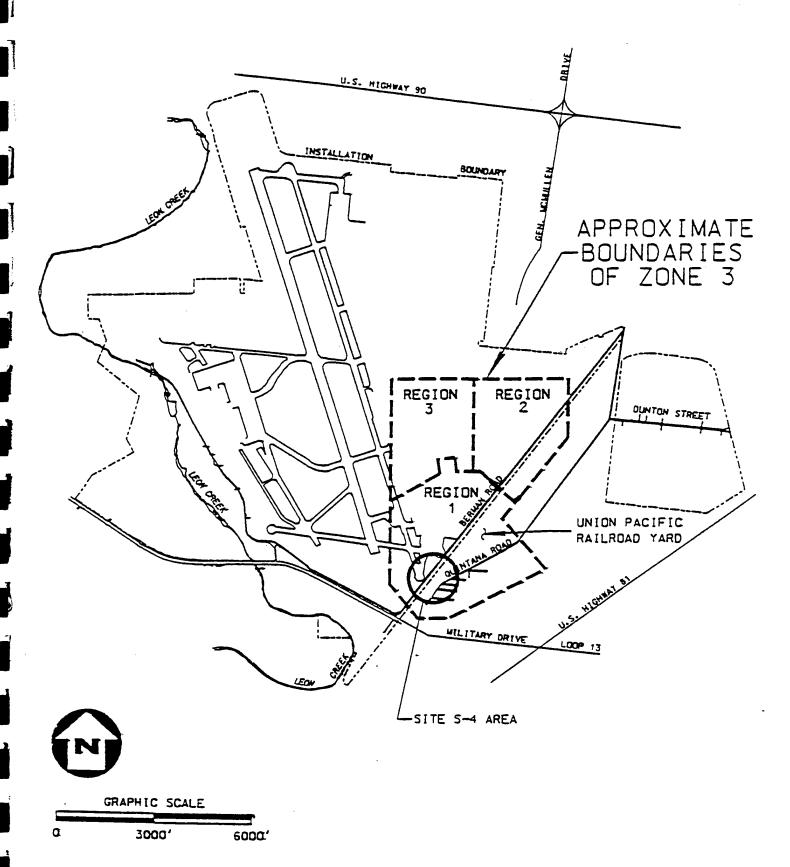


Figure 1. Schematic Diagram Showing Location of Site S-4, Kelly AFB

occurring either as randomly distributed nodules or as concentrated layers of gravel-sized nodules. This complex geological formation contributes to fluctuating groundwater depths, variable groundwater flow patterns, dry soil areas, and the apparent "pooling" of the subsurface LNAPL contamination.

# 2.2 Aquifer Characteristics

Groundwater at Site S-4 occurs at depths ranging from 14 to 16 ft bgs. In characterizing the aquifer, both slug and pump tests have been performed at the site. Results indicate that the average hydraulic conductivity of the aquifer is  $1.87 \times 10^{-2}$  cm/sec, with conductivities ranging from  $1.32 \times 10^{-1}$  cm/sec to  $1.14 \times 10^{-4}$  cm/sec (NUS 1990). Conductivity measurements at various wells are presented in Appendix B. The average transmissivity across the pump test area was calculated to be 158.2 ft<sup>2</sup>/day (NUS 1990).

The Basewide Hydrogeologic Assessment (BHA) performed by NUS in 1990 indicates that the groundwater gradient at Site S-4 generally slopes to the south-southwest. Measurements from the site surveys confirm this, but the gradient is not uniform (Figure 2). At the center of Site S-4, the gradient decreases markedly from 0.0042 ft/ft north of Z307 to 0.0014 ft/ft between Z307 and Z301 (NUS 1990). The gradient is relatively flat in the north-south direction between wells Z337 and UP05, but it steepens again south of Z317. Also noted in the NUS 1990 report was the identification of a south-southwest depression, or "channel," in the water table that crosses Site S-4.

An elevated occurrence of the Navarro clay has resulted in a dry area at Site S-4. This area affects the groundwater flow by diverting it from a southerly flow to a southwesterly direction. The groundwater gradient and the Navarro-related dry zone have been noted for playing a critical role in shaping the resulting JP-4 plume.

#### 2.3 Site Contamination

Benzene, toluene, ethylbenzene, and xylenes (BTEX) have been identified in the capillary fringe at Site S-4 at concentrations of 407 mg/kg with an average concentration of 100 mg/kg. In the area of UST F/371, soil gas measurements for total volatile hydrocarbons are reported as high as 64,000 ppmv with total BTEX levels of 543 ppmv.

The extent of the free-product plume at Site S-4, as of May 1990, is presented in Figure 3. The shape of the plume is thought to reflect the heterogeneous geology and the changeable groundwater flow and gradient. Within the JP-4 plume, three pools of free product have been identified. These pools are centered around wells S405, Z301/Z302/Z303, and Z313/Z314. Free-product thickness data is presented in Table 1. During manual bailing, well Z302 along with UP03 and Z313, consistently produced more than 3 gallons of product per half hour of continuous bailing. The field test of the bioslurper technology will likely intercept one of these 3 identified pools of free product at Site S-4. The preferred area is that associated with wells Z301/Z302/Z303 at the UPR yard off the southeastern edge of Kelly AFB, and the bioslurper pilot test will employ one of the existing recovery wells: RW02, RW03, or RW04 (Figure 4).

Estimates of total LNAPL contamination at Site S-4 have also been made in the final report on the Quintama Road Project Performance Evaluation Report for the First Four Months of Recovery System Operation at Site S-4, January 1994 (QPPE, 1994). Based upon measured fuel thickness and the areal extent of subsurface contamination, the estimated volume of JP-4 present in the formation across the plume area ranges from 150,000 to 240,000 gallons. Only a portion of the total volume will be impacted during the bioslurper test.

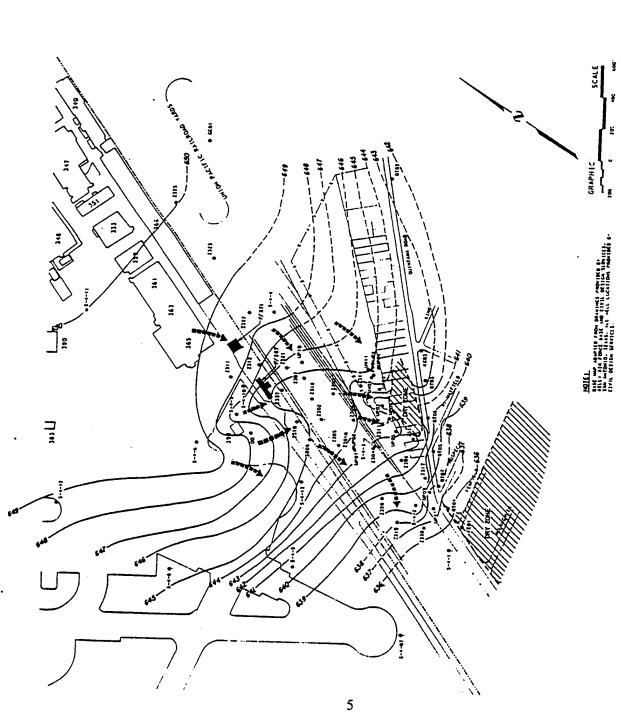


Figure 2. Groundwater Elevation and Flow Direction at Site S-4

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SITE S-4 ZONE 3 DECEMBER, 1989

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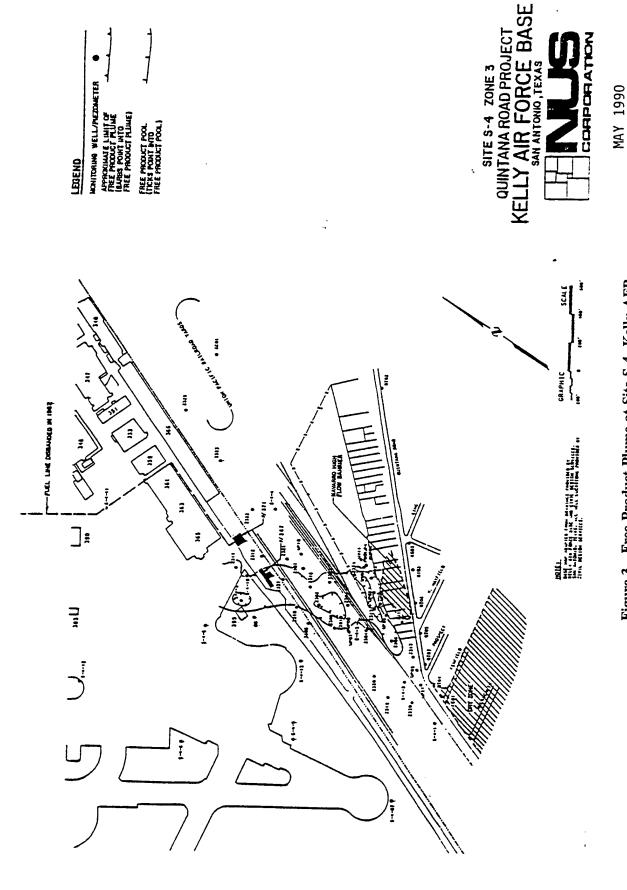


Figure 3. Free-Product Plume at Site S-4, Kelly AFB

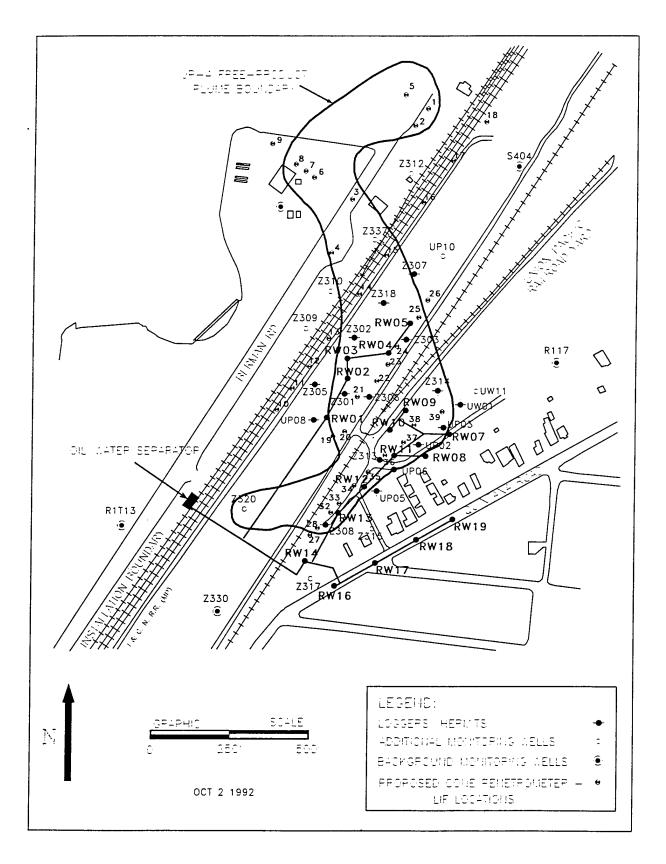


Figure 4. Location of Recovery Wells Within Site S-4

Table 1. Measured JP-4 Product Thickness at Wells Located at Site S-4

Well Number	Measured Product Thickness in Well (ft)
QT06	0.50
S405	2.25
UP02	0.49
UP03	1.13
UW09	5.70*
Z301	1.48
Z302	3.33
Z303	2.58
Z306	0.42
Z308	1.49
Z311	0.03
Z313	3.58
Z314	1.12
Z318	0.28

<sup>\* =</sup> No water in well.

#### 3.0 PROJECT ACTIVITIES

The following field activities are planned for the bioslurper pilot test at Kelly AFB. Additional details about the activities are presented in the *Test Plan and Technical Protocol for Bioslurping* (Battelle, 1995). As appropriate, specific sections in the generic Test Plan and Technical Protocol are referenced. Table 2 shows the schedule of activities for the Bioslurper Initiative at Kelly AFB.

#### 3.1 Mobilization to the Site

After the site-specific Test Plan is approved, Battelle staff will mobilize equipment. Some of the equipment will be shipped via air express to Kelly AFB prior to staff arrival. The Base Point of Contact (POC) will have been asked in advance to find a suitable holding facility to receive the bioslurper pilot test equipment so that it will be easily accessible to the Battelle staff when they arrive with the remainder of the equipment. The exact mobilization date will be confirmed with the Base POC as far in advance of fieldwork as is possible. The Battelle POC will provide the Base POC with information on each Battelle employee who will be on site. Battelle personnel will be mobilized to the site after it has been confirmed that the shipped equipment has been received by Kelly AFB.

#### 3.2 Site Characterization Tests

# 3.2.1 Baildown Tests

The baildown test is the primary test for selection of the bioslurper test well. Baildown tests will be performed at wells that contain measurable thicknesses of LNAPL (#Z301, #Z302, and #Z303) to

Table 2. Schedule of Bioslurper Test Activities

Pilot Test Activity	Schedule
Mobilization	day 1-2
Site Characterization	day 2-3
Baildown Tests and Product/Groundwater Interface Monitoring	
Soil-Gas Survey (limited)	
Slug Tests	
Monitoring Point Installation (3 MPs)	
Soil Sampling (TPH, BTEX, physical characteristics)	
System Installation	day 2-3
Test Startup	day 3
Skimmer Test (2 days)	day 3-4
Bioslurper Vacuum Extraction (4 days)	day 6-9
Soil-Gas Permeability Testing	day 6
Skimmer Test (continued) (1 day)	day 10
In Situ Respiration Test — air/helium injection	day 10
In Situ Respiration Test — monitoring	day 11-16
Drawdown Pump Test (2 days)	day 11-12
Demobilization/Mobilization	day 13-14

estimate the LNAPL recovery potential. In most cases, the well exhibiting the highest rate of LNAPL recovery will be selected for the bioslurper extraction well. Detailed procedures for the baildown tests are provided in Section 5.6 of the generic Test Plan and Technical Protocol.

# 3.2.2 Soil-Gas Survey (Limited)

A small-scale soil-gas survey will be conducted to identify the best location for installation of the bioslurping system soil gas monitoring points. The soil-gas survey will be conducted in areas where historical site data indicate the highest contamination levels. These areas will be surveyed to select the locations for installation of soil-gas monitoring points. Soil-gas monitoring points will be located in areas that exhibit the following soil gas characteristics:

- 1. Relatively high total petroleum hydrocarbon (TPH) concentrations (10,000 ppm or greater).
- 2. Relatively low oxygen concentrations (between 0% and 2%).
- 3. Relatively high carbon dioxide concentrations (depending on soil type, between 2% and 10% or greater).

To obtain further information about the soil-gas survey, consult Section 5.2 of the generic Test Plan and Technical Protocol.

# 3.2.3 Slug Tests

Slug tests will be performed to determine the characteristics of the aquifer where the candidate bioslurper test well is located (RW02, RW03, RW04). Slug tests will be performed using an in situ pressure transducer and a Hermit data logger to track pressure (water level) changes induced by a polyvinyl chloride capsule (slug) containing a known volume of water. Using the data collected during the slug test, the ability of the aquifer to recharge with water at Site S-4 will be examined. Additional information about the slug test method can be found in Section 5.7 of the generic Test Plan and Technical Protocol.

# 3.2.4 Monitoring Point Installation

Monitoring points will be installed to determine the radius of influence of the bioslurper system in the vadose zone. A general arrangement of the bioslurping well and monitoring points is shown in Figure 5.

Upon conclusion of the initial soil-gas survey and baildown tests, at least three soil-gas monitoring points will be installed to measure soil-gas changes that occur during bioslurper operation. These monitoring points should be located in highly contaminated soils within the free-phase plume and should be positioned to allow detailed monitoring of the in situ changes in soil-gas composition caused by the bioslurper system. A schematic diagram of a typical soil-gas monitoring point is shown in Figure 6. Information on monitoring point installation can be found in Section 4.2.1 of the generic Test Plan and Technical Protocol.

# 3.2.5 Soil Sampling

Soil samples will be collected to determine the physical and chemical composition of the soil near the bioslurper test site. Soil samples will be collected from the boreholes advanced for monitoring point installation at two or three locations at the site chosen for the bioslurper test. Generally, samples will be collected from the capillary fringe over the free product.

Soil samples from each boring will be analyzed for particle-size distribution, bulk density, porosity, moisture content, BTEX, and TPH. Section 5.5.1 of the generic Test Plan and Technical Protocol will be consulted for information on the field measurements and sample collection procedures for soil sampling.

# 3.3 Bioslurper System Installation and Operation

#### 3.3.1 System Setup

After the preliminary site characterization has been completed and the bioslurper candidate well has been selected, the shipped equipment will be mobilized from the holding facility to the test site, and the bioslurper system will be assembled. Figure 7 shows a flow diagram of the bioslurper process. Figure 8 is a schematic diagram of a typical bioslurper extraction well that will be installed using an existing recovery well at Kelly AFB.

Before the LNAPL recovery tests are initiated, all relevant baseline field data will be collected and recorded. These data will include soil-gas concentrations, initial soil-gas pressures, the depth to groundwater, and the LNAPL thickness. Ambient soil and all atmospheric conditions (e.g., temperature,

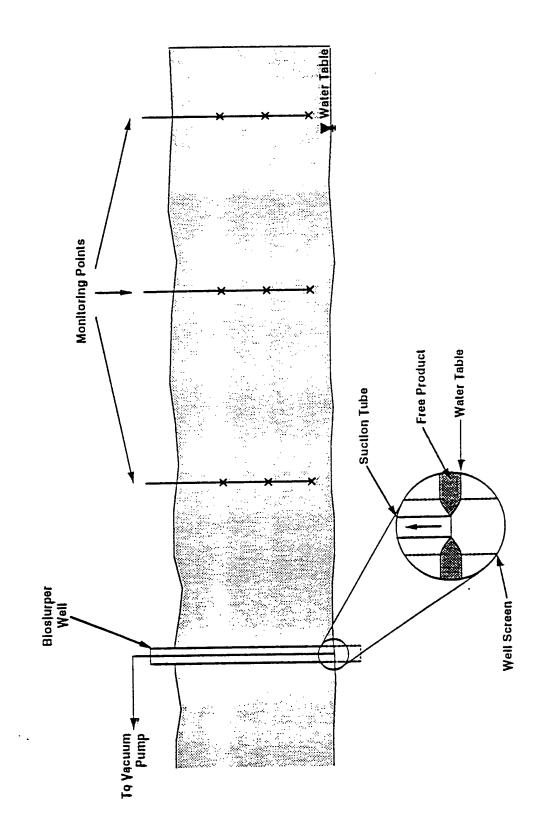


Figure 5. General Bioslurper Well and Monitoring Point Arrangement

the test, as were all other relevant data for the skimmer pump test. Test data sheets are provided in Appendix D.

# 3.4.3 Bioslurper Pump Test

# 3.4.3.1 Monitoring Well MW-11

Upon completion of the skimmer pump test, preparations were made to begin the bioslurper pump test at monitoring well MW-11. The LNAPL and groundwater depth were measured prior to any recovery testing. The slurper tube was set at the LNAPL/groundwater interface at a depth of approximately 15.7 ft bgl. The sanitary well seal was positioned inside the well, sealing the wellhead and allowing the pump to establish a vacuum in the well (Figure 5). A pressure gauge was installed at the wellhead to measure the vacuum inside the extraction well. The liquid ring pump was started at 1119, 14 November 1996, to begin the bioslurper pump test. The test was initiated approximately 4 hr after the skimmer pump test and was operated for 117.5 hr. The pump vacuum was approximately 26"Hg, the vapor flowrate from the well was approximately 72 scfm, and the well vacuum was approximately 19"H<sub>2</sub>O, and the drop tube vacuum was approximately 19"Hg. The LNAPL and groundwater extraction rates were monitored throughout the test, as were all other relevant data for the bioslurper pump test. The data sheets are provided in Appendix D.

An LNAPL sample was collected at 1300, 17 November 1997, from the oil/water separator during the bioslurper pump test and was labeled K-LNAPL-1. The sample was sent to Alpha Analytical, Inc., in Sparks, Nevada for analysis of BTEX.

#### 3.4.3.2 Monitoring Well MW-9

Upon completion of the bioslurper pump test at monitoring well MW-11, preparations were made to begin the bioslurper pump test at monitoring well MW-9. The LNAPL and groundwater depth were measured prior to any recovery testing. The drop tube was set at the LNAPL/groundwater interface at a depth of 17.8 ft below top of well casing. The sanitary well seal was positioned inside the well, sealing the wellhead and allowing the pump to establish a vacuum in the well. A pressure gauge was installed at the wellhead to measure the vacuum inside the extraction well. The liquid ring pump was started at 1308, 19 November 1996, to begin the bioslurper pump

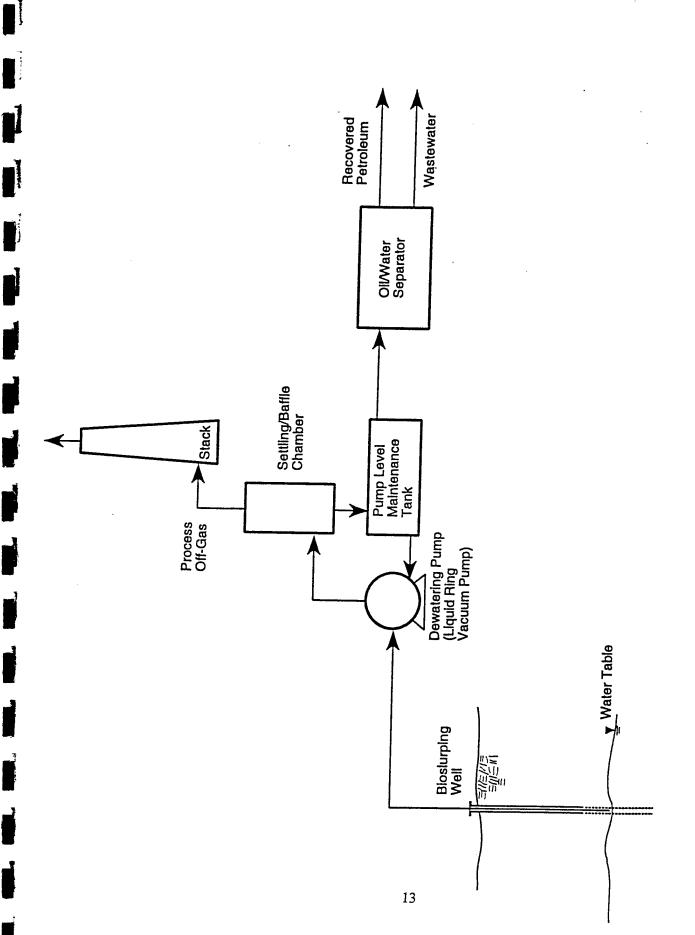


Figure 7. Bioslurper Process Flow

test. The test was initiated approximately 3 hr after the MW-11 bioslurper pump test and was operated for 23.9 hr. The pump vacuum was approximately 25.5"Hg, the vapor flowrate was approximately 82 scfm, the well vacuum was approximately 5"H<sub>2</sub>O, and the drop tube vacuum was approximately 19"Hg. The LNAPL and groundwater extraction rates were monitored throughout the test, as were all other relevant data for the bioslurper pump test. The data sheets are provided in Appendix D.

# 3.4.4 Second Skimmer Pump Test

Upon completion of the bioslurper pump test at monitoring well MW-9, preparations were made to begin the second skimmer pump test at monitoring well MW-11. Prior to test initiation, depths to LNAPL and groundwater were measured. The liquid ring pump was used to conduct the skimmer pump test with the wellhead open to the atmosphere. The drop tube was held in position at 16.5 ft below the top of the well casing. The pump was started 1445, 20 November 1996, to begin the second skimmer pump test. The test was operated for a total of 22 hr. The pump vacuum was approximately 25.5"Hg and the vapor flowrate from the well was approximately 83 scfm. The LNAPL and groundwater extraction rates were monitored throughout the test, as were all other relevant data for the skimmer pump test. Test data sheets are provided in Appendix D.

# 3.4.5 Off-Gas Sampling and Analysis

Five off-gas samples were collected during the bioslurper pump test at monitoring well MW-11. Samples KLRPV-1 and KLRPV-2 were collected from the seal tank headspace after approximately 71.5 and 102 hr of operation, respectively. Samples KICEV-1 and KICEV-2 were collected from the ICE off-gas after approximately 72 and 102 hr of operation, respectively. Sample KICEV-SP-1 was collected from the ICE sampling port after approximately 102 hr of operation. The samples were collected in Summa® canisters and sent under chain of custody to Air Toxics, Ltd., in Folsom, California, for analyses of TPH and volatile organic compounds (VOCs), using EPA Method TO-14. Analytical reports are provided in Appendix E.

# 3.4.6 Groundwater Sampling and Analysis

One groundwater sample was collected during the bioslurper pump test at monitoring well MW-11 and was labeled K-W-1. The sample was collected from the outlet to the industrial treatment plant after 76.5 hr of operation. The sample was collected in a 40-mL VOA vial containing hydrochloric acid (HCl) preservative. The sample was checked to ensure no headspace was present and was then shipped on ice and sent under chain of custody to Alpha Analytical, Inc., in Sparks, Nevada for analyses of BTEX and TPH (purgeable). Analytical reports are provided in Appendix E.

# 3.5 Bioventing Analyses

# 3.5.1 Soil Gas Permeability Testing

The soil gas permeability test data were collected during the bioslurper pump test at monitoring well MW-11. Before a vacuum was established in the extraction well, the initial soil gas pressures at the three installed monitoring points were recorded. The start of the bioslurper pump test created a steep pressure drop in the extraction well which was the starting point for the soil gas permeability testing. Soil gas pressures were measured at each of the three monitoring points at all depths to track the rate of outward propagation of the pressure drop in the extraction well. Soil gas pressure data were collected frequently during the first 20 minutes of the test. The soil gas pressures were recorded throughout the bioslurper pump test to determine the bioventing radius of influence. Test data are provided in Appendix F.

# 3.5.2 In Situ Respiration Testing

Air was injected into three monitoring points for approximately 24 hr beginning on 20 November 1996. Helium was not used due to a malfunction with equipment. The setup for the in situ respiration test is described in the Test Plan and Technical Protocol a Field Treatability Test for Bioventing (Hinchee et al., 1992). A ½-hp diaphragm pump was used for air injection. Air was injected through monitoring points MPA-12.5, MPB-13.5, and MPC-14.0. After the air/helium injection was terminated, soil gas concentrations of oxygen, carbon dioxide, and TPH were monitored periodically. The in situ respiration test was terminated on 22 November 1996. Oxygen utilization

#### 3.3.6 In Situ Respiration Tests

An in situ respiration test will be conducted after completion of the bioslurper operating tests. The in situ respiration test will involve injection of air/helium into selected soil-gas monitoring points followed by monitoring changes in concentration of oxygen, carbon dioxide, petroleum hydrocarbons, and helium in soil-gas near the injection point. Measurement of the soil-gas composition typically will be conducted at 2, 4, 6, and 8 hours and then every 4 to 12 hours for about 2 days. Timing of the tests will be adjusted based on oxygen-use rate. If oxygen depletion occurs rapidly, more frequent monitoring will be conducted. If oxygen depletion is slow, less frequent readings will be acceptable. The oxygen utilization rate will be used to estimate the biodegradation rate at the site. Further information on the procedures and data collection for in situ respiration testing is given in Section 5.8 of the generic Test Plan and Technical Protocol.

# 3.3.7 Extended Testing

The AFCEE/ERT plans to implement the option of extending the operation of the bioslurper system for up to 6 months if LNAPL recovery rates are promising and viable long-term vapor and aqueous discharge requirements have been established. When the extended testing is to be performed, the Air Force will need to provide electrical power for long-term operation of the bioslurper pump. Disposition of all generated wastes and routine operation and maintenance of the system will be the Air Force's responsibility. Battelle will provide technical support during the extended testing operation.

# 3.4 Demobilization

Once all necessary tests have been completed at the Kelly AFB site, the equipment will be disassembled by Battelle staff and will be moved back to the holding facility, where it will remain until its next destination is determined. Battelle staff will receive this information and will be responsible for shipment of the equipment to the next site before they leave Kelly AFB.

# 4.0 BIOSLURPER SYSTEM DISCHARGE

# 4.1 Vapor Discharge Disposition

Battelle expects that the operation of the bioslurper test system at the Kelly AFB site will require a waiver or a point source air release registration and may require some additional permits. Thus, a short-term (9-10 day pumping) waiver/exclusion is requested. It can be assumed that the mass of TPH released to the atmosphere will be approximately 60 lb/day and benzene will be <1.0 lb/day. This value is based on the average discharge levels at two bioslurper test sites (Wright-Patterson AFB and Travis AFB) that are contaminated with the same type of jet fuel as that found at the Kelly AFB site. The value may vary depending on soil-gas contaminant concentrations and the permeability of the soil. The data for the TPH and benzene discharge levels at four previous bioslurper sites are presented in Table 3. The relatively high TPH discharge level at Travis AFB is partially due to the presence of more permeable soils and the resultant higher extraction rate of vapors. This extraction rate is the maximum rate a 3-hp pump will achieve and will be much lower at Kelly AFB due to the lower expected permeability of the soil. The vapor stream generated by the bioslurper system can be discharged directly to the atmosphere because of the short duration of the test and the expected low concentration levels of TPH and benzene in the stream.

Table 3. Benzene and TPH Discharge Levels at Previous Bioslurper Test Sites

Site Location	Fuel Type	Extraction Rate (scfm)	Benzene (ppmv)	TPH (ppmv)	Benzene Discharge (lb/day)	TPH Discharge (lb/day)
Wright- Patterson AFB	Jet Fuel	3	ND	595	0.0	1.0
Bolling AFB (Site #1)	No. 2 Fuel Oil	4	0.2	153	0.0003	0.009
Bolling AFB (Site #2)	Gasoline	21	370	70,000	2.3	470.1
Travis AFB	Jet Fuel	20	100	10,800	0.58	126.4
Andrews AFB	No. 2 Fuel Oil	8	16	2,000	0.001	0.2

ND = Not Detected

To ensure the safety and regulatory compliance of the bioslurper system, vapor discharge samples (TPH,  $O_2$ , and  $CO_2$ ) will be collected periodically throughout the bioslurper pilot test, and field soil- gas screening instruments will be used to monitor vapor discharge concentration variability. The volume of vapor discharge will be monitored daily using air flow instruments. If state regulatory requirements will not permit the expected amount of organic vapor discharge to the atmosphere, the Base POC should inform AFCEE and Battelle so that alternative plans can be made prior to mobilization to the site. Table 4 presents information typically required to complete an air release registration form.

Table 4. Air Release Summary Information

Data Item	Air Release Information
Contractor Point of Contact	Jeff Kittel, (614) 424-6122
Contractor address	Battelle, 505 King Avenue, Columbus, OH 43201
Estimated total quantity of petroleum product to be recovered	TBD
Description of petroleum product to be recovered	JP-4 jet fuel
Planned date of test start	TBD
Test duration	9 days (active pumping)
Maximum total quantity of VOC release	~60 lb/day TPH, ~0.25 lb/day Benzene
Stack height above ground level	10 ft

# 4.2 Aqueous Influent/Effluent Disposition

The flowrate of groundwater pumped by the bioslurper during the short-term pilot test will be less than 5 gpm. In Texas, it may be necessary to obtain a groundwater pumping waiver or registration permit. If one is required, it is hereby requested.

Operation of the bioslurper system will generate an aqueous waste discharge that will be passed through an oil/water separator. The intention of Battelle staff will be to dispose of the wastewater by discharge to the on-site oil/water discharge tank currently in use. If existing Base wastewater channels can be used, no water discharge permits will be required.

# 4.3 Free-Product Recovery Disposition

The bioslurper system will recover free-phase product from the pilot tests performed at Kelly AFB. Free product recovered by the bioslurping tests will be turned over to the Base for disposal and/or recycling. Recovered free product will be transferred to existing on-site recovery tanks located within the base boundary fence. The volume of free product recovered will not be known until the tests have been performed. The maximum recovery rate for this system is 5 gpm, but the actual rate of LNAPL recovery likely will be much lower.

#### 5.0 SCHEDULE

The schedule for the bioslurper fieldwork at Kelly AFB will depend on approval of the project Test Plan. Battelle will determine a definitive schedule as soon as possible after approval is received. Battelle will have two to three staff members on site for approximately 2 weeks to conduct all necessary pilot testing. At the conclusion of the field testing at Kelly AFB, all staff will return their Base passes and will remove all bioslurper field testing equipment from the Base before they leave the site.

# 6.0 PROJECT SUPPORT ROLES

This section outlines some of the major functions of personnel from Battelle, Kelly AFB, and AFCEE during the bioslurper field test.

#### **6.1** Battelle Activities

The obligations of Battelle in the Bioslurper Initiative at Kelly AFB will be to supply the staff and equipment necessary to perform all the tests on the bioslurper system. Battelle also will provide technical support in the areas of water and vapor discharge permitting, digging permits, staff support during the extended testing period, and any other technical areas that need to be addressed.

# **6.2** Kelly AFB Support Activities

To support the necessary field tests at Kelly AFB, the Base must be able to provide the following:

a. Any digging permits and utility clearances that need to be obtained prior to the initiation of the fieldwork. Any underground utilities should be clearly marked

to reduce the chance of utility damage and/or personal injury during soil-gas probe and possible well installation. Battelle will not begin field operations without these clearances and permits.

- b. The Air Force will be responsible for obtaining Base and site clearance for the Battelle staff that will be working at the Base. The Base POC will be furnished with all necessary information on each staff member at least 1 week prior to field startup.
- c. Access to the local sanitary sewer must be furnished so that Battelle staff can discharge the bioslurper aqueous effluent directly to the Base treatment facility.
- d. Regulatory approval, if required, must be obtained by the Base POC prior to startup of the bioslurper pilot test. As stated previously, it is likely that a waiver to allow air releases or a point source air release registration will be required for emissions of approximately 60 lb/day of TPH and < 1.0 lb/day of benzene. The Base POC will obtain all necessary Base permits prior to mobilization to the site. Battelle will provide technical assistance in preparing regulatory approval documents.
- e. The Base will be responsible for the disposition of all waste generated from the pilot testing. Such waste includes any soil cuttings generated from drilling, and all aqueous wastestreams produced from the bioslurper tests. All free product recovered from the bioslurper operation will be disposed of or recycled by the Base. Battelle will provide technical assistance in disposing of the waste generated from the bioslurper pilot test.
- f. Before field activities begin, the Health and Safety Plan will be finalized with information provided by the Base POC. Table 5 is a checklist for the information required to complete the Health and Safety Plan. All emergency information will be obtained by the Site Health and Safety office before operations begin.

# 6.3 AFCEE Activities

The AFCEE POC will act as a liaison between Battelle and Kelly AFB staff. The AFCEE POC will ensure that all necessary permits are obtained and the space required to house the bioslurper field equipment is found.

The following is a listing of Battelle, AFCEE, and Kelly AFB staff who can be contacted in cases of emergency and/or required technical support during the Bioslurper Initiative tests at Kelly AFB.

Battelle POCs	Jeff Kittel Eric Drescher	614-424-6122 614-424-3088
AFCEE POC	Patrick Haas	210-536-4314
Kelly AFB POC	Ron Catchings	210-925-1812

Regulator POCs

Air:

Bill Brown

210-490-3096 ext. 330

Water:

UST: TNRCC

Table 5. Health and Safety Information Checklist

Emergency Contacts	<u>Name</u>	<u>Telephone</u> <u>Number</u>
Hospital Emergency Room:		925-3227
Point of Contact:		
Fire Department:		
	OH Base 117	925-5119
Emergency Unit (Ambulance):		925-4549
Security:	Desk Sgt.	925-6811 or 911
Explosives Unit:	Sgt. Nieholi	925-6811 or 911
Community Emergency Response Coordinator:		911 or 925-6906
Other:		
Program Contacts To be notified in case of eme	ergency	
Air Force: AFCEE		
Base	Patrick E. Haas	210-536-4314
	Ron Catchings	210-925-1812
Battelle:	Jeff Kittel	614-424-6122
	Eric Drescher	614-424-3088
Emergency Routes		
Hospital (Maps attached)		
Other:		

# APPENDIX A

GEOLOGICAL CROSS-SECTIONAL PROFILES
AND A SUMMARY OF GEOTECHNICAL DATA FOR SITE S-4

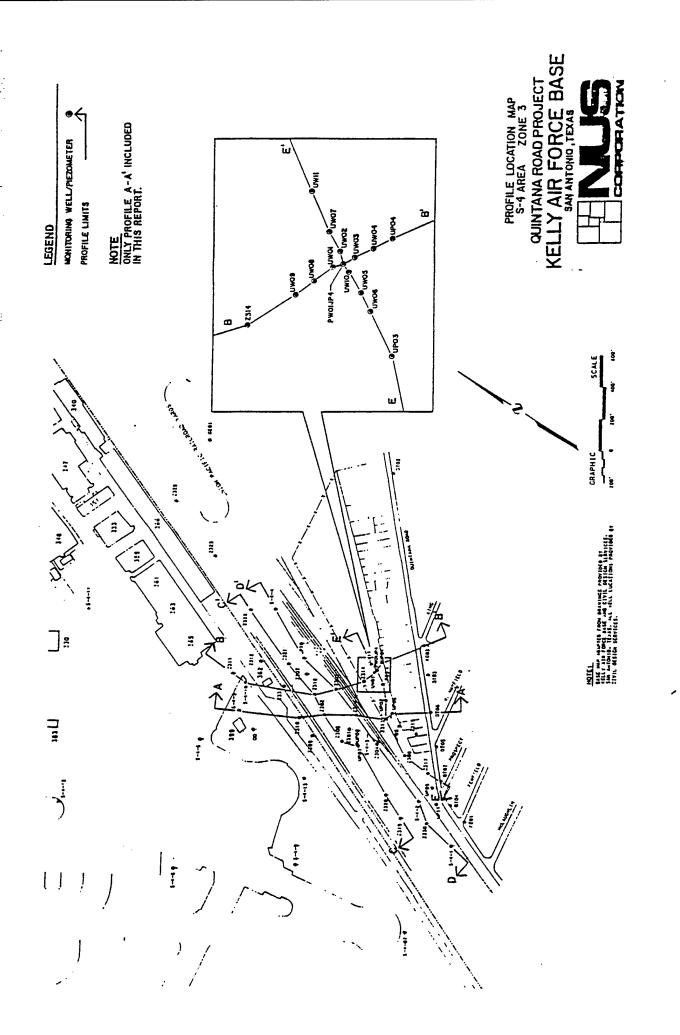


Figure A-1. Profile Location Map S-4 Area Zone 3

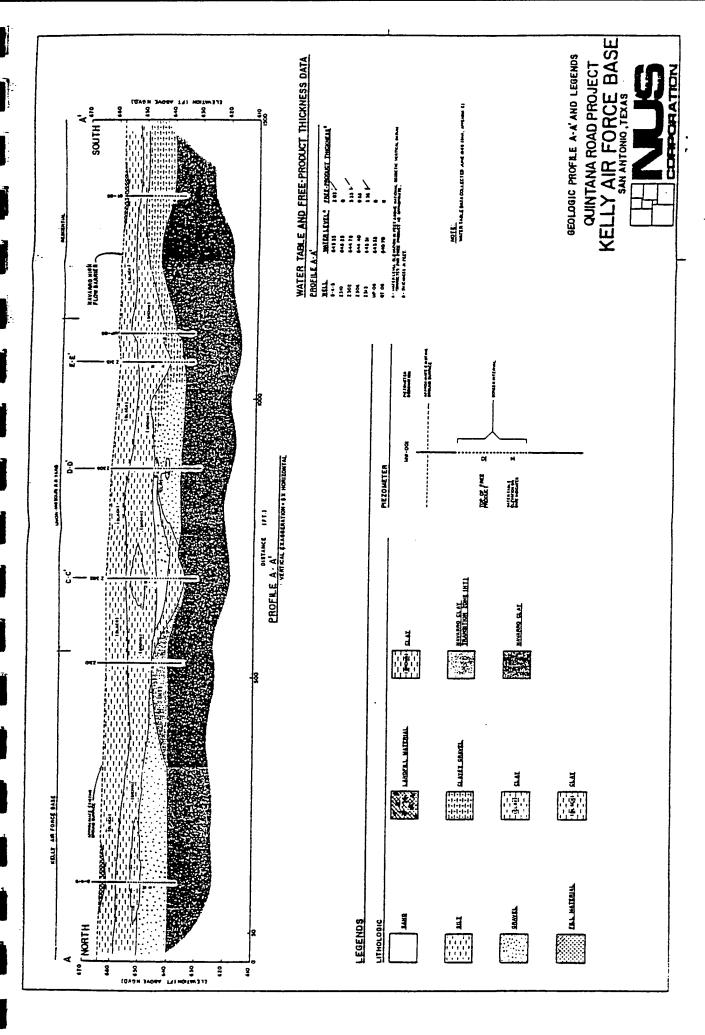


Figure A-2. Geologic Profile A-A'

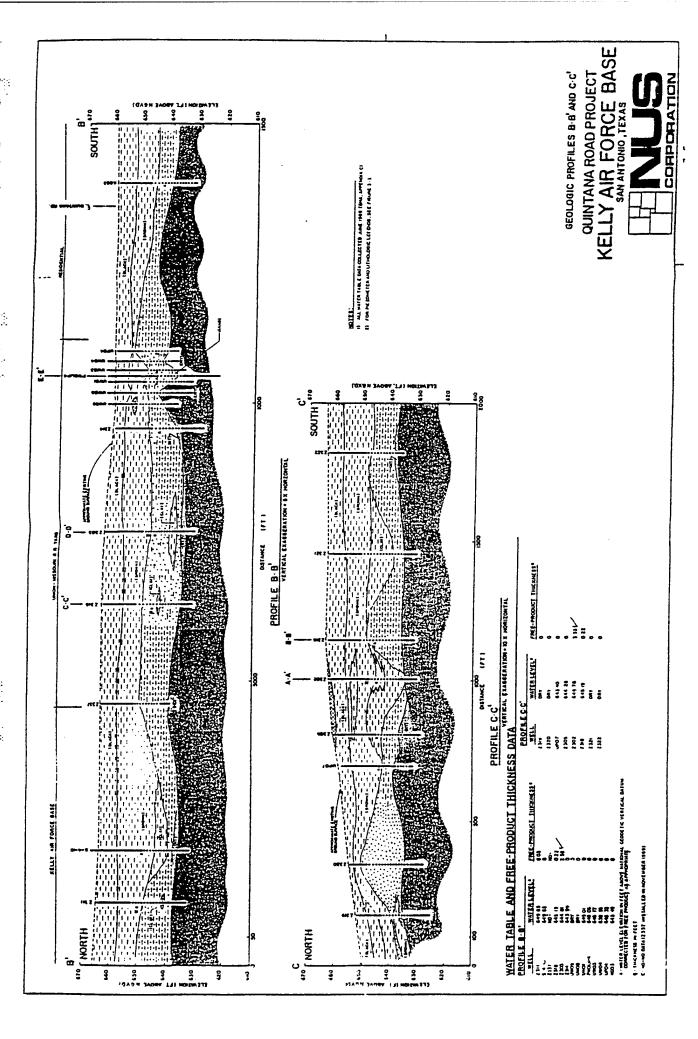


Figure A-3. Geologic Profiles B-B' and C-C'

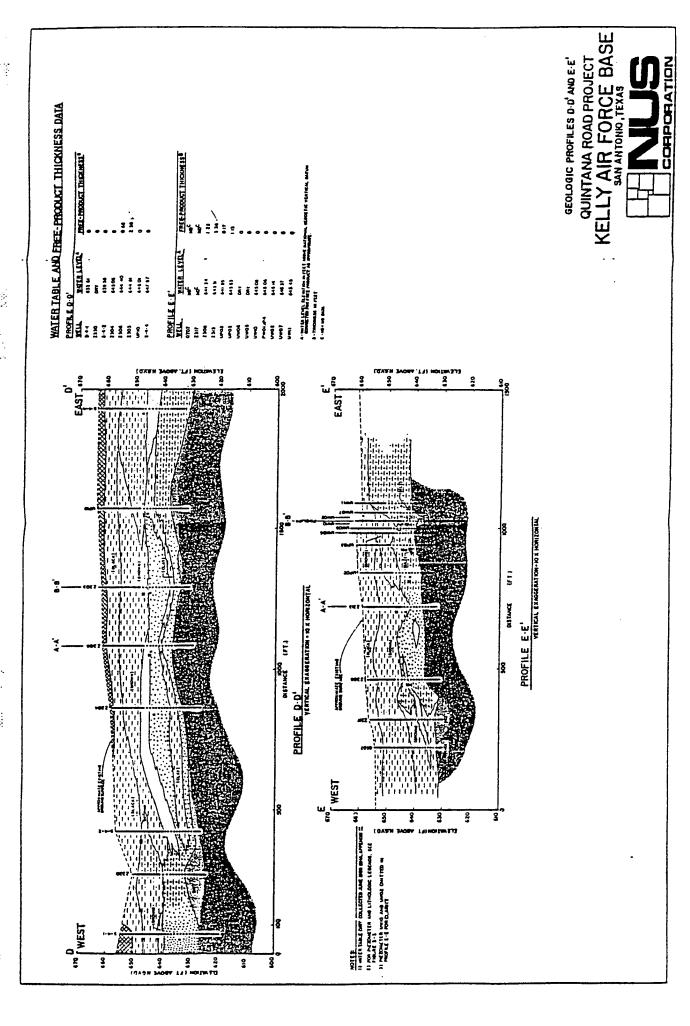


Figure A-4. Geologic Profiles D-D' and E-E'

# SUMMARY OF GEOTECHNICAL DATA QUINTANA ROAD PROJECT

┝╾┼╴	1082	2302	Z303	2305	2306	7307	2318
		17-18	17-18	17-19	17-19	25-27	5.7
Brown Clay/ Br Gravel(b)	ğ ,	Brown Clay/ Gravel(b)	Brown Clay/ Grave((b)	Clayey Gravel	Gravel	Clayey Gravel/ Gravel(b)	Black Clay/
2.59		2.61	2.53	2.62	2.63	2.71	273
7.7		7.5	16.0	14.9	14.9	11.2	20.4
0 0026	)	0.0018	0.0012	0.015	0.029	0 057	NB
4.33 × 10·5 3.0	3.0	3.00 × 10·5	2.0 × 10·5	2.5 x 10-4	4.83 x 10.4	9 50 × 10-4	1 5 x 10.7
1.88		1.80	1.33	1.51	1.66	1.77	1.52
8.4		8.4	8.3	8.4	8.7	8.7	NR
396		396	377	399	401	408	aN
Sm or SC SM o	SM	or SC	ML, CL, MH, CH	SM or SC	SM or SC	GM-SM or GC-SC	aN
89 8	6	8.7	NR	81.7	0 96	92.0	014
72.2 89.	æ	9.1	NR	70.0	80.0	68.0	YAY OZ
68.4 8	8	86.7	92.9	65.2	69.5	53.3	7 99
61.1 8	8	80.0	87.6	54.3	42.9	38.0	97.6
54.8	7	6.07	85.5	47.9	27.2	29.2	02.7.0
46.4	LS.	58.4	82.2	43.2	19.5	21.7	933.1
38.1		47.5	75.0	38.0	17.3	18.4	5.25 NB
33.6		42.3	NR	34.5	NR.	NR	86.7
					T		

Note: NR - Not reported.

(a) Unified soil classification system.
(b) The sample interval crosses the lithofacies boundary.

Table A-1. Summary of Geotechnical Data Quintana Road Project

# APPENDIX B

AQUIFER CONDUCTIVITY MEASUREMENTS AND PUMP AND SLUG TEST DATA FOR SITE S-4

# HYDRAULIC CONDUCTIVITY AT MONITORING WELLS IN THE QUINTANA ROAD PROJECT AREA(a)

Monitoring Well/ Piezometer	Hydraulic Conductivity cm/sec
KG-03	1.32 x 10-i
00	2.41 x 10-3
PW01 JP-4	9.05 x 10-3
QT03	3.08 x 10-3
UP02	3.09 x 10-2
UP03(b)	1.2 x 10 <sup>-1</sup>
UP04	1.14 x 10 <del>-4</del>
UP05	1.56 x 10- <sup>3</sup>
UP07(c)	9.84 x 10-6
UP08	1.09 x 10-3
UP10	3.12 x 10-3
UP11	4.49 x 10-2
UW01	5.15 x 10-3
UW02	1.78 x 10-2
UW03	1.42 x 10-3
UW07	3.56 x 10 <sup>-2</sup>
UW10	9.16 x 10 <sup>-2</sup>
UW11	2.72 x 10-2
Z304	1.69 X 10 <sup>-2</sup>
Z305	6.59 X 10 <del>-4</del>
Z307	1.49 X 10-2
Z309	7.46 X 10-4

Monitoring Well/ Piezometer	Hydraulic Conductivity cm/sec
Z311	5.91 X 10-3
Z312	2.66 X 10-3
Z314	. 7.15 X 10-3
Z317	3.84 X 10-3
Z318	3.38 X 10-4
Z319	4.35 x 10 <sup>-3</sup>
Z320	9.96 x 10-3
Z321	4.45 x 10 <sup>-3</sup>
Z322	4.25 x 10-3
Z323	1.06 X 10 <sup>-1</sup>
Z325	4.13 x 10-2
Z330	5.19 x 10-3
S-4-1	7.47 x 10-4
S-4-2	2.7 x 10 <sup>-3</sup>
S-4-3	5.9 x 10 <sup>-2</sup>
5-4-4	1.3 x 10-3
5-4-7	6.50 x 10-4
S-4-8	1.22 x 10 <sup>-2</sup>
5-4-9	4.02x 10-2
S-4-10	2.13 x 10-4
S-4-11	1 26 x 10-2
5-4-12	1.34 x 10 <sup>-1</sup>

Note: All values derived from aquifer slug tests except where noted.

Bouwer, H. and R.C. Rice. 1976. "A Slug Test for Determining Hydraulic Conductivity of Unconfined Aquifers with Completely or Partially Penetrating Wells." Water Resources Research, V12(3).

<sup>(</sup>a) Hydraulic conductivity was calculated using the method of Bouwer and Rice (1976).

<sup>(</sup>b) Hydraulic conductivity determined from pump test data.

<sup>(</sup>c) Piezometer installed with a five foot PVC screen within the Navarro clay.

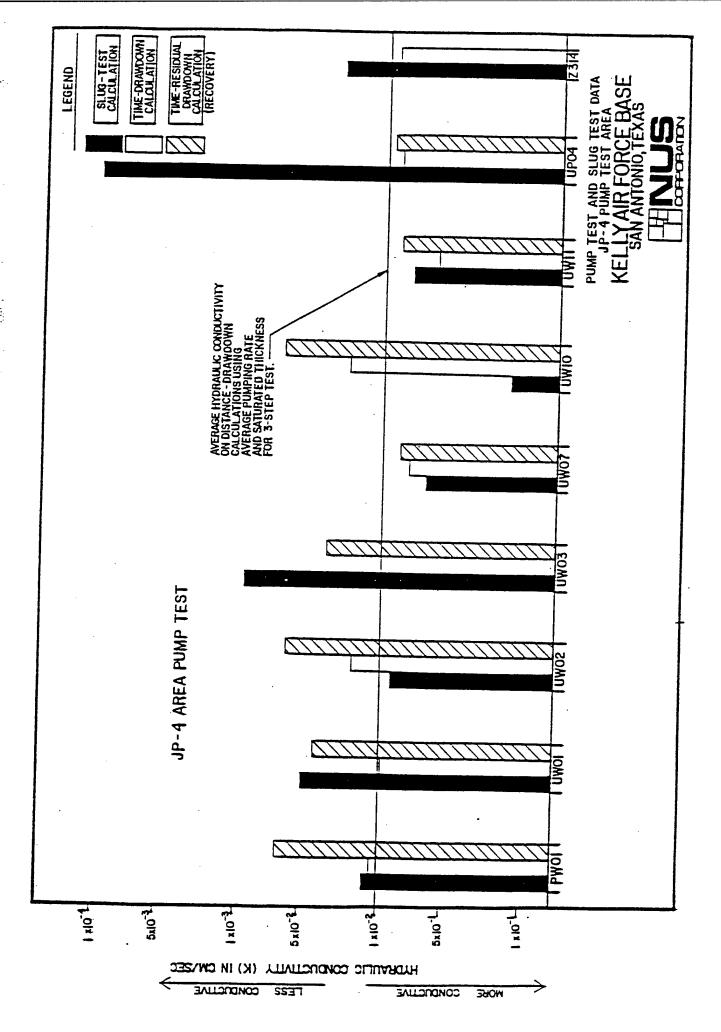


Figure B-1. Pump Test and Slug Test Data JP-4

APPENDIX B

ICE OPERATIONAL DATA

ESTART AT: 11/12/96 11:36:20 (11/08/96 08:36:39) S5245 V2.23 . 1/12/96 11:36:23 UNIT 182 4. 75.F 77.F 84.F 0. 16.8 -0.7 Ø. 12. 12.6 99.9 0.500 0.00 356 1394. 100 115 /12/96 11:37:18 UNIT 182 75.F 85.F 77.F Ø. 19.0 -0.7 Ø. 12. 12.6 99.9 0.500 0.00 115 356 1394. <u> 2</u>ESTART AT: 11/12/96 11:38:33 (11/12/96 11:38:12) 85245 V2.23 /12/96 11:38:11 UNIT 182 75.F 77.F 85.F 23.5 **-0.**7 8. Ø. 0. 12. 12.1 78.2 0.544 115 356 1394. 0.00 11/12/96 11:38:36 UNIT 182 4. 75.F 77.F 85.F Ø. 23,5 **-0.**7 0. 12. 12.6 99.9 0.500 0.00 356 1394. 115 ESTART AT: 11/12/96 11:40:08 (11/12/96 11:38:52) 55245 V2.23 11/12/95 11:40:11 UNIT 182 0. 99.9 0.500 1394. 4. 75.F 77.F 86.F 23.5 12. 12.6 0.00356 100 Ø. *-0.*7 115 京28786時は41855片UNITy9922/9分711941:55%(25.612/86 1歩f.40:38) 55245.700V2の3高 - 115 1394. 356

ESTART AT: 11/12	2/96	11:44	1:28	(11/12	2/96	11:4	2:56)	<b>S</b> 52	45 V:	2.23	E.		
11/12/96 11:44:31 UNIT 182 100 4. 75.F 77.F	86.F	100.	23.5	<b>-0.</b> 7	Û,	12.	12.6	99.9	0.500	0.00	115	356	1394.
1/12/96 11:45:43 UNIT 192 :00 1590. 97.F 78.F	400.F	53.	23.6	-0 <b>.</b> 7	ŵ.	12.	13.7	10.3	0 <b>.</b> 679	0.00	115	356	1394.
11/12/96 12:00:06 UNIT 181													
0 1865. 160.F 158.F 1/12/96 12:01:33 UNIT 191	831.F	53.	23.4	-1.0	0.	14.	13.2	10.2	0.680	0.00	115	356	1394.
100 2329, 161,F 159,F	937.F	53.	23.4	-1.1	ŷ,	14.	13.3	10.1	0.680	0.85	115	357	1394.
00 2401. 154.F 161.F	903.F	53.	23.4	-1.0	Ø.	14.	13.3	51.8	0.594	0.73	115	358	1394.
11/12/96 12:03:00 UNIT 182 100 2403. 165.F 164.F	917 <b>.</b> F	53.	23,4	-1,0	Ø.	14.	13.3	50.3	0.599	0.72	115	358	1394.
1/12/96 12:03:52 UNIT 191 30 2198. 164.F 166.F	930 <b>.</b> F	53.	21.2	-1.0	0.	14.	13.2	54.4	0.591	0.90	115	359	1394.
11/12/95 12:04:10 UNIT 162	607 C	53.	17.9	-1.0	Ø.	14.	13.3	59.2	0.582	ø.81	115	359	1394.
0 1852. 164,F 166,F 712/96 12:04:49 UNIT 182	923.F	JJ.											
190 1843. 164.F 166.F	998.F	53.	17.9	-1.0	Ø.	14.	13.3	59.2	0.582	0.00	115	359	1394.

V.R.SYSTEMS INC.

MODEL V3 S/N 182 PERMIT NO.

ENGINE TEMPERATUR		OIL Pai		TIONS BYPABS	WELL CFM-VA		BATTERY VOLTS	DUTY CVCLE	PERCENT OXYGEN		.IARY FU )USANDS-		ENGINE HOURS
RPM COOLANT OIL	EXHAUST	Lai	UHNS.	DIFHEE	CEMEAN	iu:MZU	AAFIS	LIGGE	DVIDER	CHI HA	10001120	OKT 10	1120110
1/12/94 12:05:35 UNIT 182													
20 1849. 163.F 165.F	872 <b>.</b> F	53.	17.5	-1.0	0,	14.	13.4	53.7	0.593	0.73	115	360	1394.
11/12/96 12:06:40 UNIT 181	-,, <del>-</del>		74 A	+ A	Δ	4.8	17 5	49.6	0.601	2.10	115	363	1395.
00 2253. 163.F 164.F	366.F	53.	21.0	-1.0	∅.	14.	13.4	47.0	A.OA1	2.10	110	500	1470.
1/12/96 12:07:08 UNIT 181 100 2278. 164.F 165.F	887.F	53.	21.0	-0,5	ø.	14.	13.5	51.6	0.597	2.46	115	364	1395.
41/12/95 12:07:40 UNIT 182	22												
00 2236. 165.F 165.F	899.F	53.	21.0	-0.9	0.	14.	13.4	50.9	0.598	2,53	115	365	1395.
1/12/96 12:08:27 UNIT 182													
100 2223. 165.F 166.F	901 <b>.</b> F	53.	21.0	-0.9	θ.	14.	13.5	49.9	0.600	2.50	115	367	1395.
1/12/96 12:09:15 UNIT 182 0 2209. 166.F 167.F	903.F	53.	21.0	-0.9	0.	14.	13.5	51.1	0.598	2.48	115	369	1395.
₩9 2209. 166.F 167.F 11/12/96 12:10:12 UNIT 181	7₩3.F	⊍ಬ.∗	Z1:V	Ve/	V:	471	7010	U1:1	41010	21:0	***	20:	10:01
±00 2170. 166.F 167.F	909.F	53.	18.9	-0.8	18.	14.	13.5	49.5	0.601	2.50	115	372	1395.
1/12/96 12:11:03 UNIT 182													
100 2200. 166.F 168.F	909.F	53.	15.6	-0.7	38.	13.	13.5	48.7	0.603	2.50	115	374	1395.
11/12/96 12:13:28 UNIT 181	56 <b>7 F</b>	E7	45 O	-0.5	53.	13.	13.5	50.0	0.600	2.43	115	380	1395.
00 2200. 166.F 169.F 1/12/96 12:14:48 UNIT 181	903.F	53.	12.8	~ღ.კ	۽ ٺِل	10.	19*4	40.0	8:000	4.70	110	000	10/01
100 2184. 166.F 169.F	906.F	53.	12.8	-0.5	53.	13.	13.5	49.3	0.601	2.43	115	383	1395.
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00 2232. 165.F 170.F	892.F	53.	5.9	9.0	94.	12.	13.1	50.3	0.599	2.51	115	391	1395.
11/12/96 12:19:58 UNIT 181													
100 2222. 165.F 171.F	889.F	53.	-0.4	12.8	113.	11.	13.3	52.6	0.595	2.54	115	396	1395.
1/12/96 12:27:47 UNIT 181	007 C	57	_0.4	12.8	113.	12.	13.2	52.9	0.594	2.54	115	416	1395.
→ 100 2197. 167.F 174.F 11/12/96 12:29:25 UNIT 181	887.F	53.	-∅,4	14.0	110.	14:	10.4	<i>04.</i> 17	V.U/T	4:07	120	710	12101
<b>1</b> 00 2200. 167.F 174.F	888.F	53.	-0,4	12.8	113.	12.	13.2	52.0	0.596	2.55	115	421	1395.
1/12/96 12:30:00 UNIT 182													
100 2210. 167.F 174.F	887.F	53.	-0,4	12.8	113.	12.	13.1	51.5	<b>0.597</b>	2.54	115	422	1395.
1/12/96 12:31:29 UNIT 181							47.5	F0 F	A 500	n =#	4+5	857	170=
00 2204. 169.F 175.F	887.F	53.	-0.4	12.9	113.	12.	13.2	50.5	0.599	2.54	115	425	1395.
T1/12/96 12:42:40 UNIT 181 100 3167. 169.F 176.F	914,5	53.	-Ø, <b>∆</b>	14.3	119.	11.	13.1	53.8	0,592	2.10	115	453	13 <b>0</b> 5.
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11/12/96 1 <b>2:</b> 47:03 UNIT 181													
<b>168.</b> F 175.F	934.F	53.	<b>-</b> ∅,4	15.2	122.	11.	13.1	52.9	0.594	2.22	115	467	1375.
1/12/96 <b>12:</b> 52:00 UNIT 181													
100 2158. 168.F 175.F	935.F	53.	-0.4	15.4	122.	11.	13.1	52.0	0.596	2.23	115	474	1395.
1/12/96 12:57:39 UNIT 182								r:	4 55:			407	: TRE
00 2151. 168.F 175.F	946.F	53.	-0.4	15.9	125.	10.	13.1	51.8	0.576	2.27	115	487	1395.
T1/12/96 13:00:00 UNIT 181	040.5	<b>27</b>	G A	4 & 4	125.	10.	13.1	52.0	0.596	2.30	115	493	1395.
100 2167. 168.F 175.F	949.F	53.	-0.4	16.1	î di vî s	IV.	10:1	32.0	V • J 7 G	4.00	110	774	10/01
1/12/96 13:30:00 UNIT 18I	947.F	53.	-Ø.4	16.1	124.	13.	13.0	52.5	0.595	2.32	115	564	1396.
00 2201. 170.F 177.F 11/12/96 14:00:00 UNIT 18I	74/∗Γ	وتول	~₩. <del>1</del>	10.1	147:	101	1417	O. L. O.	Vau/v	せいひて	115	20°	10:01
######################################	946.F	53.	-0.4	16.1	125.	13.	13.1	53.1	0.594	2.31	115	635	1396.
1/12/96 14:30:00 UNIT 181			• • •										
100 2193. 169.F 176.F	947.F	53.	-0.4	16.2	124.	12.	13.1	53.1	0.594	2.31	115	706	1397.
11/12/96 15:00:00 UNIT 182													
00 2194. 169.F 177.F	947.F	53.	-0.4	16.1	124.	12.	13.0	54.0	0.592	2.31	115	777	1397.
/12/96 15:30:00 UNIT 182													
100 2179. 169.F 176.F	947.F	53.	-0.4	16.1	124.	12.	13.1	53.4	0.593	2.30	115	848	1398.
1/12/96 16:00:00 UNIT 182					453	45	47 4	<b>-</b> a	A 664	5 71	445	010	1398.
0 2214. 169.F 177.F	945.F	53.	-0,4	16.1	124.	12.	13.1	54.4	0.591	2.31	115	919	1370.
17/12/94 17:00:00 UNIT 182	511 5	==	Δ 4	47.4	103	+=	+7.0	E7 7	0.593	2.32	115	60	1399.
100 2186. 169.F 175.F	944.F	53.	-0,4	16.1	124.	12.	13.2	53.3	V.373	Z.J.Z	110	54	1077.

V.R.SYSTEMS INC. MODEL VJ S/N 181 PERMIT NO.

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ı	7.71.2	CODLAHT	<u> </u>	EXHAUST	FII	CARD.	Daff of	A **#	. ~	**	- *	. <del>.</del> '	- "	1.177	arritti (†	HittiAf
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1	∸je žže5.		. 73 <b>.</b> F	945.F	53.	-0.4	la.V	174.	i2.	13.2	52.6	0.595	2.29	116	342	1401.
	/12/96 19:		IT 182	547 F		0.4		124.	12.	13.3	54.1	0.592	2.29	116	385	1402.
	100   2215. 11/12/96 19:	168.F		943.F	53.	-0.4	16.2	124.	14.	10.0	J# . 1	V.J7Z	4.47	110	984	1704.
j	19 2221.	168.F	174.F	943.F	53.	-0.4	16.2	124.	12.	13.2	53.6	0.593	2.29	116	385	1402.
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	100 2205.		173.F	945.F	53.	-0.4	16.2	124.	12.	13.2	54.4	0.591	2.29	116	483	1402.
	/12/96 21:			545 5	E7	A #	47 4	124.	12.	13.2	52.8	0.594	2.28	116	623	1403.
ı	0 2218. 11/12/96 22:	168.F	172.F IT 181	745.F	53.	-0.4	16.1	124.	14.	10.2	J4:0	V.J74	7.70	110	020	14691
	11/12/75 22: 100 2206.	168.F	171.F	946.F	53.	-Ø.4	16.2	124.	12.	13.3	52.9	0.594	2.30	116	764	1404.
	/12/96 23:						, - · · ·									
١		147.F	171.F	943.F	53.	-0.4	16.0	123.	12.	13.3	51.9	0.57£	2.27	iiá	903	1405.
,	11/13/96 00:			515 5			47.0	107	10	17 7	52.7	0.595	2.28	117	42	1406.
1	0 2189.	168.F		942.F	53.	-0.4	16.0	123.	12.	13.3	JZ./	₩.073	4.40	117	44	1400.
1	/13/96 01: 100 2187.		IT 182 170.F	943.F	53.	-0.4	16.0	123.	12.	13.3	53.9	0.592	2.27	117	181	1407.
	11/13/95 02:			, , , , ,												
	e 21 <b>78.</b>	167.F	169.F	744.F	53.	-ē.4	iá.i	123.	i2.	13.2	52.4	0.595	2.26	117	320	1498.
	11/13/96 03:		IT 181				4: 5	451	4.0	47.7	E+ E	A E07	2.27	117	459	1409.
1	100 2184.	167.F		944.F	53.	Ø.4	16.0	124.	12.	13.3	51.5	<b>0.59</b> 7	L. 41	11/	437	1407.
	,/13/96 04: ₩A 2178.	168.F	IT 182 171.F	942.F	53.	-0.4	16.1	123.	i2.	13.2	54.0	0.592	2.27	117	597	1410.
•	11/13/96 05:		IT 181	, , , , , ,					<b>-</b>							
1	M 2173.	140.F	171.F	942.F	53.	-\$. <del>4</del>	iś.i	123.	12.	13.3	52.4	0.595	2.27	117	735	1411.

730 Am 11-13-96

/13/96 05:26:56 UNIT 181	941.F	53.	-0,4	16.0	124.	12.	13.3	54.0	0.592	2,27	117	798	1412.
## 2164. 168.F 171.F 11/13/96 05:27:18 UNIT 182	771.5	de,	-v.+	18.0	127:	14.5	1010	V 7 # 4	01012	4.14.	+	,,,,	1:111
<u>19</u> 0 2163. 168.F 171.F	941.F	53.	-0.4	16.0	123.	13.	13.3	54.6	0.591	2.25	117	798	1412.
1/13/96 05:44:44 UNIT 181													
₹60 2184. 169.F 171.F	943.F	53.	-0.4	16.0	123.	13.	13.3	52.9	<b>0.594</b>	2.27	117	839	1412.
11/13/96 @5:47:10 UNIT 181				47.4	157	13.	i3.3	52.7	0.595	2.27	117	844	1412.
## 2158. 168.F 171.F	941.F	53.	-0,4	16.0	123.	13.	10.0	34.7	v.373	2.27	117	577	1712.
1/13/95 06:00:00 UNIT 181	943.F	53.	-0.4	16.0	124.	13.	13.2	52.5	0.595	2.24	117	874	1412.
₩ /13/96 06:30:00 UNIT 181													
00 2171. 168.F 171.F	945.F	53.	-0,4	16.1	124.	13.	13.3	53.0	0.594	2.25	117	943	1413.
T1/13/96 07:00:00 UNIT 182										- : <del>-</del>			
490 2169. 168.F 172.F	941.F	53.	-9.4	16.0	124.	13.	13.1	53.5	<b>0.59</b> 3	2.17	118	12	1413.
1/13/96 07:30:00 UNIT 181 00 2161. 168.F 174.F	961.F	53.	-0.4	17.0	129.	13.	13.1	53.0	0.594	2.28	118	81	1414.
11/13/96 08:00:00 UNIT 181	1011	00.	V. 1	1710	±±/•	15.							
<b>1</b> 9 2171. 168.F 175.F	766.F	53.	-0.4	17.4	132.	13.	13.1	52.7	0.595	2.34	118	153	1414.
/13/96 08:30:00 UNIT 182													
100 2175. 169.F 176.F	967.F	53.	-0.4	17.4	131.	13.	13.0	53.7	0.593	2.33	118	225	1415.
11/13/96 09:00:00 UNIT 181 0 2200. 169.F 177.F	969.F	53.	-0.4	17.7	132.	13.	13.0	56.2	0,588	2.39	118	298	1415.
71/13/96 09:30:00 UNIT 182	1011	<i>ರ</i> ಚ ಕ	¥∗ा	4/1/	100;	10:	1010	0012	01000	210,			
196 2182. 169.F 177.F	970.F	53.	-0.4	17.7	133.	13.	13.1	54.6	0.591	2.37	118	371	1416.
10:00:00 UNIT 182													
A 9109. 178.F 178.F	972.F	53.	-0.4	17.8	134.	13.	i3.i	53.9	0.592	2.39	118	444	1416.
11/13/96 11:00:00 UNIT 182	577.5			45.5	475	40	17 1	55.2	0.590	2.41	118	593	1417.
140 2189. 169.F 178.F	977 <b>.</b> F	53.	-0.4	18.2	135.	12.	13.1	Ų <b>J</b> ∗Δ	V.J7V	4.71	110	9/4	171/:

V.R.SYSTEMS INC.

MODEL V3 S/N 182 PERMIT NO.

ENGINE	TER	4PERATI	JRE	OIL	POS1	ITIONS	WELL	FLOW	BATTERY	DUTY	PERCENT		LIARY FU		ENGINE
RPK	COOLANT	OIL	EXHAUST	PSI	CARB.	BYPASS	CFM-V	AC.H2O	VOLTS	CYCLE	OXYGEN	CFM TH	IDUSANDS-	-UNITS	HOURS
/13/96 11: 100 2185.	171 <b>.</b> F	IT 182 177.F	977 <b>.</b> F	53.	<b>-</b> ∅,4	18.2	135.	12.	4	53.8	0.592	2.43	118	613	1418.

100 2140. 1/1.6 1/6.6	¥/5.F	J.;	-8.4	18.1	130.	12.	13.2	54.9	0.070	2,44	116	513	i+lö.
≟4/13/96 12:00:00 UNIT 182													
14 5175 175 F 126 F	978.F	53.	-8.4	18.2	136.	12.	13.0	53.7	0.593	2.44	118	742	1418.
100 2218. 170.F 180.F	924.F	53.	-0.5	15.2	121.	13.	13.0	58.0	0.584	2.43	118	892	1419.
100 1100 1700 1700 1800 1800 1800 1800 1	, _ ,	001	V10	1012	1221		1010	20.0	0100:	11.0	**-		* . * . *
<b>5</b> € 2192. 171.F 180.F	921 <i>.</i> F	52.	-0.4	15.0	120.	13.	13.1	56.6	0.587	2.44	119	41	1420.
11/13/96 14:52:39 UNIT 182	007.5	E 7	Α. ε	4E A	115	10	17 1	E/ 5	A E00	O 47	110	171	1421.
66 2209. 170.F 179.F 713/96 15:00:00 UNIT 182	923.F	53.	-0,4	15.0	117.	12.	13.1	56.2	v.588	2.43	119	171	1941:
100 2217. 170.F 179.F	922.F	53.	-0,4	15.0	120.	12.	13.1	56.8	0.586	2.41	119	189	1421.
_11/13/96 16:00:00 UNIT 182													
## 2211. 169.F 177.F 	720.F	53.	-0.4	14.8	117.	12.	13.1	t.6t	0.587	2.40	117	336	1422.
100 2217. 169.F 176.F	919.F	55.	-0.5	14.7	119.	12.	13.1	56.9	0.586	2.38	119	385	1423.
📆/13/96 16:20:31 UNIT 182						_							
0 2202. 169.F 176.F	919.F	55.	-0.5	14.7	117.	12.	13.1	57.2	0.586	2.39	119	386 -	1423.
11/13/96 17:00:00 UNIT 182 <u>10</u> 0 2166. 168.F 174.F	905.F	55.	-0.5	13.8	116.	12.	13.0	56.1	0.588	2.33	119	484	1423.
/13/96 18:00:00 UNIT 182													
90 2166. 167.F 173.F 11/13/96 19:00:00 UNIT 183	909.F	53.	-0.4	14.0	117.	12.	13.2	54.7	0.591	2.31	119	626	1424.
21710745 17109108 GRI: 161	910.F	53,	~~ (j , 4	14.1	117.	12.	13.3	54.6	0.591	2.30	119	747	1425.
/13/96 20:00:00 UNIT 181													
100 2143. 167.F 172.F 41/13/96 20:16:14 UNIT 182	911.F	53.	-0,4	14.0	117.	12.	13.3	54.1	0.592	2.28	119	908	1426.
0 2148. 167.F 171.F	911.F	53.	- <b>0.4</b>	14.1	117.	12.	13.4	56.6	0.587	2.29	119	946	1427.
11/13/96 20:16:26 UNIT 182													
100 2154, 167.F 171.F	911.F	53.	-0.4	14.1	117.	12.	13.3	54.5	0.591	2.29	119	947	1427.
/13/96 21:60:00 UNIT 182 & 2163. 167.F 171.F	912.F	55.	-0,4	14.1	117.	12.	13.5	55.4	0.587	2.29	120	49	1427.
11/13/96 22:00:00 UNIT 182			•••										
##0 2161. 167.F 170.F	911.F	53.	-⊕.4	14.1	117.	12.	13.5	55.7	0.587	2.29	120	187	1428.
/13/96 23:00:00 UNIT 182 100 2178. 167.F 170.F	911.F	53,	-0,4	14.1	117.	11.	13.5	52.5	0.595	2.29	120	329	1429.
<u>11</u> /14/96 00:00:00 UNIT 182		• • •											
# 2159. 167.F 170.F	912.F	53.	-0.4	14.1	117.	ii.	13.6	53.2	0.594	2.27	120	469	1430.
1/14/96 01:00:00 UNIT 182 100 2167. 167.F 170.F	911.F	53.	-0.4	14.2	117.	ii.	13.6	53.8	0.592	2.27	120	608	1431.
/14/96 02:00:00 UNIT 182			<b>31</b> ,		**/*								2,227
9 2168. 167.F 169.F	914.F	53.	-0,4	14.2	116.	11.	13.6	54.1	0.592	2.26	120	747	1432.
11/14/96 03:00:00 UNIT 182	912 <b>.</b> F	53.	-0.4	14.2	117.	11.	13.6	53.7	0.593	2.28	120	856	1433.
/14/96 04:00:00 UNIT 182	,				• • • •	•••	10.0		****				
100 2179. 167.F 169.F	913.F	53.	-0.4	14.5	118.	iē.	13.6	52.9	0.394	2.28	i2i	25	1434.
11/14/96 05:00:00 UNIT 182 0 2170. 168.F 170.F	915.F	53.	-0.4	14.5	117.	11.	13.6	54.0	0.592	2.28	121	165	1435.
174/76 05:22:17 UNIT 182	w . :	201	w # 1			:							
100 2172. 167.F 169.F	919.F	53.	-0,4	14.6	118.	11.	13.6	53.5	0.593	2.29	121	216	1436.
★ /14/96 05:22:24 UNIT 182 ② 2172. 167.F 169.F	919.F	53.	-0.4	14.6	118.	ii.	13.6	53.7	<b>0.59</b> 3	2.27	121	217	1436.
11/14/95 06:00:00 UNIT 181													
190 2171. 167.F 170.F	917.F	53.	-0,4	14.6	118.	11.	13.5	52.8	0.574	2.28	121	304	1436.
V.R.SYSTEMS INC.	12	יין ופתחו	S/N 181										
, v.n.atalino 196.		SEMIT N											

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ENGINE	TEMPERATI		01L		TIONS	WELL	FLOW	BATTERY	DUTY	PERCENT			JEL	ENGINE
RPM	COOLANT OIL	EXHAUST	PSI	CARB.	BYPASS	: '- :: - ::	AC.H20	VOLTE	CYCLE	DXYGEN	: ::-	OUSANDS:	_::::::	HOURE
/14/96 07: 0 2165. 1/14/96 08:	168.F 171.F	918.F	53.	-0.4	14.7	119.		13.4	53.2	0.594	2.33	121	444	1437.

100 2101. 107.F 1/0.F	740.5	ودي	~#.+	idei	2.47 s			Lugar	v	47		*	.7
#1/14/96 05:33:19 UNIT 181   186   2218.   147.5		=											
ry 2216. 1271: 1													
					117.	17.	131.4	LELY	0.1346	2.64	121	672	1439.
	212 6	e=	Δ 4	iz a	100	45	4 <del>.</del> .	50 4	A ED/	0.77	101	, <del>77</del>	1.75
# 175.F 11/14/96 08:36:11 UNIT 182	917.F	53.	-∅.4	15.0	120.	12.	13.4	52.1	0.596	2.66	121	673	1439.
<b>168.</b> F 175.F	917.F	53.	-0.4	15.0	119.	12.	13.5	52.1	0.596	2.64	121	674	1439.
1/14/96 09:00:00 UNIT 182													
700 2208. 169.F 176.F	914.F	53.	-0.4	14.9	119.	12.	13.4	54.2	0.592	2.62	121	737	1439.
11/14/96 07:15:32 UNIT 182 00 2156. 167.F 176.F	931.F	53.	-0.4	16.3	124.	11.	13.3	52.2	0.596	2.64	121	779	1440.
-1/14/96 09:33:04 UNIT 182	741:5	od:	थ≛न	10.0	147.0		2010	VA SA	010.0	210:		, , ,	1::01
100 2197. 170.F 177.F	912 <b>.</b> F	53.	-0.4	14.9	119.	12.	13.3	54.3	0.591	2.54	121	824	1440.
1/14/96 09:40:10 UNIT 182			0.4		4.5		4 <del>- 1</del> 1	E/ 5	A 500	7 FA	101	047	1 A A C
90 2194. 168.F 177.F 11/14/96 10:00:00 UNIT 182	911 <b>.</b> F	53.	-0.4	15.0	119.	12.	13.4	56.2	0.588	2.50	121	843	1440.
11/14/76 10:00:00 URL 161 400 2217. 170.F 178.F	915.F	52,	-0.4	15.0	119.	12.	13.3	54.5	0.587	2.68	121	895	1440.
/14/96 11:00:00 UNIT 182													
₹00 2188. 170.F 178.F	915.F	52.	<b>-</b> 0,4	15.0	119.	11.	13.3	54.9	0.590	2.67	122	57	1441.
11/14/96 11:53:12 UNIT 182 10 2201. 171.F 180.F	918.F	52.	-0,4	15.3	120.	11.	13.3	56.8	0 <b>.</b> 586	2.68	122	202	1442,
1/14/96 12:00:00 UNIT 182	11511	46.1	V.7	1010	2201		1010	0010	*****	2100	***-		a 1 , au 3
100 2197. 172.F 181.F	916.F	52.	-0.4	15.2	120.	11.	13.2	58.2	0.584	2.58	122	220	1442.
<b>1</b> /14/96 12:11:17 UNIT 182													1443.14:116
90 2201. 171.F 180.F	919.F	52.	-0.4	15.2	120.	11.	13.3	54.9	0.570	2.68	122	250	1443. [7.1)
11/14/96 12:11:26 UNIT 182 100 2210. 171.F 180.F	919.F	52.	<b>-</b> ∅,4	15.2	120.	11.	13.3	55.4	0.569	2.65	122	250	1443.
/14/96 12:11:33 UNIT 182													
<b>4</b> 0 2200. 171.F 180.F	919 <b>.</b> F	52.	-0,4	15.2	120.	11.	13.3	54.5	0.591	2.67	122	251	1443.
11/14/96 12:12:41 UNIT 183	545 5		5 A	4 <b>2</b> 7	150	4 4	17.7	55 5	a ====	5 /=	122	254	1443.
70 2206. 171.F 180.F 1/14/96 12:13:11 UNIT 182	918.F	52.	-0.4	15.3	120.	11.	13.3	55.5	0.589	2.65	122	20*	1990:
100 2198, 171.F 180.F	918 <b>.</b> F	52.	-0.4	15.2	120.	11.	13.3	56.9	Ø.586	2.65	122	255	1443.
₩/14/95 13:00:00 UNIT 182													
0 2191. 171.F 181.F	919.F	52.	-0.4	15.3	120.	11.	13.2	58.1	0.564	2.62	122	386	1443.
100 2205. 171.F 181.F	9 <u>1</u> 9.F	52.	-0,4	15.2	120.	10.	13.3	56.4	0.587	2.61	122	489	1444. Remove.
/14/96 14:00:00 UNIT 182	7 - 7 - 1	¥4.1	V # T	1012	2201	101	1010	0011	0.00.	2101	• • • •		HOTUST
0 2197. 171.F 179.F	920.F	52.	-0.5	15.2	120.	10.	13.2	56.2	0.588	2.60	122	540	1446. A
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	,													
	:15:36 UNII 1dZ										·		554	4055
<u></u> 2175.	170.F 179.F	917 <b>.</b> F	52.	-0.4	15.1	119.	10.	13.4	56.9	0.586	2.51	122	581	1445.
<b>188</b>	:00:00 UNIT 182	5/5 5	50	6. <i>1</i> .	4 E A	445	9.	13.3	57.7	0 505	2.56	122	697	1445.
T00 2182.	170.F 177.F	918.F	52.	<b>-</b> ∅,4	15.0	119.	7.	10.0	Q/ a/	0.585	Z:30	177	Q7/	1440:
	:00:00 UNIT 182									1 27 20 20			557	2551
0 2180.	170.F 178.F	918 <b>.</b> F	52.	-0,4	15.1	119.	10.	13.3	57.7	0.585	2.57	122	853	1446.
	:00:00 UNIT 181				4		4.5	47.7	F, .	A 500		107		4 5 5 7
	169.F 177.F	918.F	52.	<b>-</b> ∅.4	15.0	119.	10.	13.3	56.1	0.588	2.55	123	9	1447.
	:00:00 UNIT 182												, , ,	4 0 05
0 2195.	169.F 176.F	919.F	52.	-0.4	15.0	119.	10.	13.3	57.0	0.584	2.52	123	164	1448.
•	:45:39 UNIT 182								·					4445
<b>110</b> 0 2205.	168.F 176.F	919.F	52.	-0.4	15.0	119.	10.	13.5	57.6	0.585	2.53	123	281	1449.
-														
_														
V.R.SYS	TEMS INC.	:	MODEL V	3 S/N 18	<b>1</b> 2									
		:	PERMIT !	NO.										
ENGINE	TEMPERATU	RE	GIL	FOSI	TIONS	WELL	FLOW	BATTERY				LIARY F		ENGINE
RPM	CODLANT CIL	EXHAUST	PSI	CAR9.	BYPASS	CFM-V	AC.H20	VOLTS	CYCLE	OXYGEN	CFM TH	iOUSANDS	-UNITS	HOURS
_														
/14/96 19:	190:00 UNIT 182													
<del>_</del> 0 2193.	169.F 175.F	919.F	53.	-0, đ	15.0	119.	10.	13.0	57.1	0.586	2.53	123	318	1449.
11/14/95 20	:00:00 UNIT 181													
<b>2</b> 207.	148.F 174.F	919.F	52.	-Ø, Å	15.1	119.	10.	13.5	54.2	0.592	2.50	123	471	1450.
/14/96/21:	100:00 UNI 197													
	168.F 173.F	918.F	52.	-∅.4	15.1	119.	10.	13.5	56.5	0.587	2.49	123	624	1451.
	:00:00 UNIT 182													
Ø 2192.	168.F 173.F	920.F	52.	-0.3	15.1	119.	9.	13.5	55.4	0.589	2.51	123	776	1452.
	:00:00 UNIT 183													
<u>10</u> 0 2193.	167.F 172.F	921.F	52.	-2.1	15.9	122.	9.	13.6	55.1	0.590	2.47	123	927	1453.
/15/96 00	:00:00 UNIT 18I													
<b>4</b> 0 2202.	167.F 172.F	921.F	53.	-2.2	15.9	122.	9.	13.6	53.2	0.594	2.49	124	78	1454.
11/15/96 01	:00:00 UNIT 182													
	168.F 172.F	920.F	53.	-2.2	15.9	122.	Ω <sub>7</sub> .	13.6	53.5	0.593	2.47	124	229	1455.
	:00:00 UNIT 183													
T00 2195.	168.F 172.F	919.F	53.	-2.2	15.9	123.	9.	13.6	54.9	0.590	2.47	:24	380	1456.
<b>53</b> /15/96 03	:00:00 UNIT 18I													
₩ 21 <b>9</b> 5.	168.F 173.F	919.F	53.	-2.2	15.9	122.	9.	13.6	55.5	0.589	2.49	124	531	1457.
<b>-</b> 1/15/96 04	:00:00 UNIT 181													
100 2213.	167.F 171.F	920.F	53.	-2.2	15.9	123.	9.	13.6	54.9	0.570	2.45	124	682	1458.
/15/95 05	:00:00 UNIT 181													
9 2192.	167.F 171.F	920.F	53.	-2.2	15,7	123.	3.	13.6	53.6	0.593	2.44	124	832	1459.
	:38:41 UNIT 181											. = -		
	167.F 172.F	720.F	53.	-2.2	15.9	122.	₽.	13.7	54.1	0.592	2.45	124	929	1460.
	:38:51 UNIT 192													
700 2195.	167.F 172.F	920.F	5J.	-2.2	15.9	123.	8.	13.7	52.4	0.595	2.47	124	929	1460.
	:38:59 UNIT 182			<b>.</b> .	,	,	_		em o	A 250	n 17	150	674	18/6
0 2194 <b>.</b>	167.F 172.F	920.F	53.	-2.2	15.9	123.	8.	13.7	JJ.0	0.594	2.47	124	930	1460.

11.15.4

11/15/96 06:00:00 UNIT 182 00 2203. 168.F 171.F	920.F	53.	-2.2	15.9	123.	ē.	13.6	54.6	0.591	2,44	124	982	1460.
1/15/96 07:00:00 UNIT 182 100 2190. 169.F 173.F	917.F	52.	-2.3	15.8	122.	9.	13.6	55.7	0.589	2.47	125	132	1461.
11/15/96 08:00:00 UNIT 182 00 2175. 170.F 176.F	916.F	52.	-2.3	15.8	122.	9.	13.4	55.4	0.589	2.46	125	283	1462.
-1/15/96 09:00:00 UNIT 182 100 2165. 169.F 176.F	916.F	52.	-2.3	15.8	122.	7.	13.4	54.8	0.590	2.46	125	434	1463.
1/15/96 09:41:47 UNIT 182 00 2167. 170.F 177.F	915.F	52.	-2.3	15.8	122.	8.	13.4	56.5	<b>0.</b> 587	2.50	125	540	1464.
11/15/94 10:00:00 UNIT 182 100 2153. 148.F 174.F	915.F	52,	-2.2	15.8	122.	8.	13.5	56.3	0.587	2.48	125	586	1464.
1/15/96 11:00:00 UNIT 182 .00 2189. 169.F 175.F	922.F	52.	-2.2	16.0	123.	7.	i3.5	54.4	4.371	2.59		730	
11/15/96 11:12:25 UNIT 192 140 2170. 147.F 175.F	923.F							18.1		. • •	. "	4 =4	letā.
	.11.F	e 3 7. •	-2.2	18.0		7.	13.5	54.7	0.591	2,53	170	891	1466.
12/15/96 13:00:00 UHIT III pe 2:00. : :::::::::::::::::::::::::::::::	922.F	53.	-2.2	16.0	124.	7.	13.4	54.0	0.592	2.50	126	43	1467.
T1/15/96 14:00:00 UNIT 182 100 2185. 170.F 176.F	921 <b>.</b> F	53.	-2.2	16.0	124.	7.	13.4	54.1	0.592	2.51	126	176	1468.
1/15/96 15:00:00 UNIT 182 60 2191. 169.F 177.F	922.F	52.	-2.2	16.0	124.	7.	13.4	54.6	0.591	2.55	126	350	1469.
11/15/96 16:00:00 UNIT 183 ■####################################	923.F	53.	-2.2	16.0	124.	7.	13.5	53.4	0.593	2.50	126	503	i470.
1/15/96 17:00:00 UNIT 182 100 2197. 168.F 175.F	923.F	53.	-2.2	16.0	124.	7.	13.4	53.3	0.593	2.51	126	656	1471.

V.R.SYSTEMS INC. MODEL V3 S/N 182 PERMIT NO.

	ENGINE	TEI	MPERATU	RE	OIL	POSI	TIONS	WELL	FLOW	BATTERY	DUTY	PERCENT	AUXII			ENGINE
	RPK	COOLANT	OIL	EXHAUST	PSI	CARB.	BYPASS	CFM-VA	C.H20	VOLTS	CYCLE	OXYGEN	CFM TH	IUSANDS-	UNITS	HOURS
-																
	15/96 18:		IT 182	007 E	E7	2.2	47 4	104	7.	13.5	55.3	0.587	2.50	126	807	1472.
NO.		167.F	174.F	923.F	53.	-2.2	16.1	124.	1 :	10.0	dusu	0.001	2:00	170	QV.	11/41
100	/15/96 18: : 2181.	169.F	IT 182 175.F	923.F	54.	-2.3	16.0	123.	7.	13.0	56.5	0.587	2.51	126	835	1473.
	: 2101. (15/96 18:		173.F IT 182	720.5	J7.	ت • ش	1010	2. A. W.	, ,	1010	50.0	31007				*
		149.F	175.F	923.5	55.	-2.3	iá.0	123.	7.	13.1	54.9	<b>0.58</b> 6	2.50	126	836	1473.
Ţ.,	15/96 19:		IT 182													
100	2184.	168.F	175.F	924.F	53.	-2.2	16.0	123.	7.	13.3	55.5	0.589	2.50	126	962	1473.
/		•	IT 182						_			5 F5:	5 45			1.474
100	2168.		174.F	924.F	53.	-2.2	16.1	124.	7.	13.3	54.7	0.591	2.48	127	114	1474.
	15/96 21:		T 182	<del>-</del>	53.	-2.2	16.0	124.	7.	13.3	56.1	<b>4.588</b>	2.5i	127	266	1475.
			175.F IT 182	924.E	JJ.	-2.2	10.0	127.		13.3	35.1	0.000				1
168			175.F	924.F	53.	-2.2	16.0	124.	7.	13.2	56.0	0.588	2.51	127	419	1476.
	15/96 23:		IT 182													
:0		169.F	175.F	923.F	53.	-2.2	16.0	123.	7.	13.2	55.9	0.588	2.49	127	571	1477.
11/	16/96 00:	00:00 UN	IT 182													
taa	7140	140 E	175 F	977.F	<b>=</b> ,₹	-7.7	14,1	<u> </u>	7.	13.3	55,4	0,559 	2.51	127	724	1478.

11/16/96 01:00:00 UNIT 182	923.F	53,	-2.2	16.1	123.	7.	13.3	55.1	0 <b>.</b> 590	2.49	127	876	1479.
2170. 169.F 175.F /16/96 02:00:00 UNIT 182	723.5	<i>ರವ</i> ಕ	-4.4	10.1	120.	<i>I</i> •	10.0	<u>ಬಿಬಿಕತಿ</u>	W.0/V	4:71	127	976	117:1
100 2167. 168.F 175.F	924.F	53.	-2.2	16.0	123.	Ġ.	13.3	55.2	0.590	2.48	128	29	1480.
11/16/96 03:00:00 UNIT 182 8 2:54. 149.F 175.F	923.F	53.	-2.2	14.0	123.	á.	13.2	55.4	a.589	2.48	128	181	1481.
71/16/96 04:00:00 UNIT 182				25.4		٠.	1012						
100 2178. 168.F 175.F	923.F	53.	-2.2	16.0	124.	7.	13.3	55.8	0.588	2.50	128	333	1482.
/16/96 05:00:00 UNIT 182 0 2163. 168.F 174.F	922.F	53.	-2.2	ić.i	124.	á.	13.3	55.6	0.589	2.47	128	484	1483.
11/16/96 05:38:43 UNIT 182	, 22 2 .												
2176. 168.F 175.F	923.F	53.	-2.2	16.0	123.	ć.	13.3	56.8	0.586	2.45	128	582	1484.
/16/96 05:38:50 UNIT 182	923.F	53.	-2.2	16.0	123.	6.	13.3	56.3	0.587	2.47	128	582	1484.
11/16/96 06:00:00 UNIT 182								5; S	A F5:	5 45	400	, <del>-</del> ;	4 45 4
0 2169. 168.F 175.F ./16/96 07:00:00 UNIT 182	923.F	53.	-2.2	16.1	123.	6.	13.3	56.8	0.586	2.48	128	636	1484.
100 2164. 169.F 176.F	921.F	53.	-2.2	16.0	124.	7.	13.2	55.3	0.587	2.47	128	788	1485.
16/96 08:00:00 UNIT 182	007 C	53.	-2.2	16.1	124.	7.	13.2	56.7	0.587	2.52	128	940	1486.
0 2156. 169.F 177.F II/16/96 09:00:00 UNIT 182	923.F	uu.	-7:7	10:1	124:	<i>( *</i>	10.4	5 <b>Q.</b> 1	W:001	2102	120	772	14001
<u>10</u> 0 2143. 169.F 178.F	926.F	53.	-1.8	16.4	125.	7.	13.2	57.3	0.585	2.55	129	74	1487.
/16/96 10:00:00 UNIT 182 0 2163. 170.F 177.F	926.F	53.	-2.2	16.3	125.	ć.	13.0	56.4	0.587	2.56	129	259	1488.
11/16/96 11:00:00 UNIT 182	720.5	J.J.,	-4.4	10.0	1201	U.	1010	2017	01007	2100	11.	200	1,001
<b>☆</b> // 2161. 172.F 182.F	931.F	52.	-2.2	16.7	126.	6.	13.0	58.1	0.584	2.63	129	407	1489.
/16/96 11:38:19 UNIT 182 100 2166. 175.F 183.F	930.F	52.	-2.4	16.1	127.	5.	13.0	58.1	0.584	2.63	129	508	1490.
12/14/75 11:30:34 1HIT 192	70011	UL.	2.7	1011	**** / \$	V.	2010		01001	1,00	•••		• •
e 2170. 175.F 183.F 93	50.F 52	2	2.4 1	6.0 i	26.	5. 13	3.1 5	9.i 0.	582 2	1.63 i	29	509 1	490.
_													
1													
-													
44/16/96 12:00:00 UNIT 182 0 2156. 173.F 182.F	932 <b>.</b> F	52.	-2.4	16.5	126.	5.	13.0	54 A	<b>0.5</b> 87	2.62	129	566	1470.
0 2156. 173.F 182.F 11/16/96 13:00:00 UNIT 182	732.7	ůř.	-2.4	15.4	140.	Ú.	1617	0010	veuus		·	550	41/4#
-AA 5127 - 175 E - 185 E	070 E	55	_7 A	14.5	177	Ξ.	17 1	50.5	a Sot	2,59	199	725	1491.

14/16/96 12:00:00 UNIT 182 0 2156. 173.F 182.F 11/16/96 13:00:00 UNIT 182	932 <b>.</b> F	52.	-2.4	16.5	126.	5.	13.0	56.6	0.587	2.62	129	566	1470.
160 2163. 172.F 182.F	932.F	52.	-2.4	16.5	127.	5.	i3.i	58.5	0.583	2.59	129	725	1491.
/16/96 14:00:00 UNIT 182 0 2168. 173.F 183.F	931.F	52.	-2.4	16.5	126.	6.	13.1	58.2	Ø <b>.</b> 584	2.62	129	884	1492.
11/16/96 15:00:00 UNIT 182 2165. 172.F 181.F	930.F	52.	-2.3	16.5	127.	6.	13.1	59.6	0.581	2.59	130	42	1493.

HODEL VI S/W 182 PERMIT NO.

ENGI	NE TE	MPERATL	RE	OIL	P051	TIONS	WELL	FLOW	BATTERY	DUTY	PERCENT			JEL	ENGINE
R.F	M COOLANT	OIL	EXHAUST	PSI	CARB.	BYPASS	CFM-VA	ŀC.H2O	VOLTS	CYCLE	OXYGEN	CFM TH	OUSANDS-	-UNITS	HOURS
/16/98	16:00:00 UN	NT 182													
100 217		180.F	932.F	52.	-2.3	16.5	127.	6.	13.1	59.1	0.582	2.56	130	200	1474.
<del></del>		VIT 182						,		55 4	A 504	5 5/	476	75/	1.105
9 217		179.F	934.F	53.	-2.2	16.5	127.	6.	13.2	58.1	0.584	2.56	130	356	1495.
		178.F	935.F	53.	-2.2	16.6	127.	٨.	13.2	57.1	0.586	2.56	130	430	1496.
100 217		1/0.r (IT 182	733.5	J.) .	~7.2	10*0	14/1	0.	10.4	07.1	0.000	7100	100	754	17701
0 216	2. 169.F	178.F 178.E	935.F	53.	-2.2	16.6	127.	6.	13.3	58.3	0.583	2.55	130	431	1496.
13A 747			ਹੁੰਦਰ ਹ	==		11 1	- ==			<u> </u>	5 ###	D 51	• <del>-</del>	, <del>* ** *</del>	* * 2 5

11/16/96 17:30:12 UNIT 182													
0 2162. 170.F 178.F	935.F	53.	-2.2	16.6	127.	6.	13.2	59.2	0.582	2.57	130	435	1496.
	935.F	53.	-2.2	16.6	127.	6.	13.2	58.0	0.584	2.56	130	435	1476.
1/16/96 18:00:00 UNIT 182 0 2171. 169.F 178.F	936.F	54.	-2.3	16.5	127.	6.	13.1	58.4	0.583	2.56	130	513	1496.
11/16/96 19:00:00 UNIT 182 100 2161. 168.F 177.F	935.F	52.	-2.2	16.6	127.	7.	13.2	57.6	0.585	2.55	130	669	1497.
1/16/96 20:00:00 UNIT 182	936 <b>.</b> F	52.	-2.2	16.6	127.	7.	13.1	58.1	0.584	2.55	130	824	1498.
11/16/96 21:00:00 UNIT 182	935.F	53.	-2.2	16.7	127.	7.	13.2	57.8	0.584	2.55	130	980	1499.
/16/96 22:00:00 UNIT 182 100 2157. 169.F 178.F	935.F	53.	-2.2	16.7	127.	ē.	13.3	58.0	ø.584	2.53	131	135	1500.
本/16/96 23:00:00 UNIT 182 編 3475. 169.5 137.5	933.E	==	-2.2	14.7	127.	ā.	13.2	58.8	8.522	2.53	131	290	1501.
11/17/96 00:00:00 UNIT 152	934.F	53.	+2.2	16.7	128.	ē.	13.2	58.1	0.584	2.53	131	444	1502.
717/96 01:00:00 UNIT 182 8 2103 889.5 878.5	934.E	53.	<u>-5,                                    </u>	14.5	1551	<u>.</u>	11.1		1.724	9.53	131	772	1265.
11/17/96 02:00:00 UNIT 182	936.F	53.	-2.1	16.8	127.	6.	13.3	56.2	0.588	2.51	131	752	1504.
17/76 03:00:00 UNIT 182 100 2192. 169.F 176.F	936 <b>.</b> F	53.	-1.6	16.8	128.	8.	13.3	58.3	0.583	2.51	131	706	1505.
11/17/96 04:00:00 UNIT 182 10 2187. 168.F 175.F	739.F	53.	-i.5	16.8	128.	8.	13.2	57.1	0.586	2.51	132	69	1504.
4/17/96 05:00:00 UNIT 182	936.F	53.	-1.5	16.8	128.	9.	13.2	56.2	0.588	2.51	132	214	1507.
100 2177. 169.F 176.F 177.96 05:39:20 UNIT 182						9.	13.3	57.0	0.586	2.51	132	315	1508.
00 2182. 169.F 176.F 11/17/96 05:39:27 UNIT 182	938.F	53.	-1.6	16.8	128. 128.	7. 9.	13.3	57.8	0.584	2.51	132	315	1508.
190 2193. 169.F 176.F 1/17/96 06:00:00 UNIT 182	937.F	53.	-1.6	16.8									
100 2193. 168.F 175.F 11/17/96 07:00:00 UNIT 182	939.F	53.	-1.6	16.8	128.	<b>7.</b>	13.3	57.2	0.586	2.51	132	368	1508.
00 2187. 169.F 177.F 1/17/96 08:00:00 UNIT 181	935.F	53.	-1.6	16.8	128.	9.	13.2		0.587	2.50	132	521	1509.
100 2202. 167.F 170.F	931.F	53.	-2.3	iá.á	126.	9.	13.5	<u>14.6</u>	8.572	2,44	132	<u> </u>	
# 22#1. 187.F 178.F	722.7			i									
							TALL	164.7	01.1AY	V.4V	LW	971	1512.
1/17/96 12:00:00 UNIT 182	925.F	53.	-2.3	16.3	126.	9.	13.5	53.9	0.592	2.44	133	120	1513.
0 2197. 169.F 174.F	926.F	53.	-2.3	16.3	125.	7.	13.4	55.2	0.590	2.46	133	270	1514.
V.R.SYSTEMS INC.	M	ODEL VO	5 8/N 183	<u>.</u>									
•	Pi	ERMIT N	<b>0.</b>										
ENGINE TEMPERATU RPM COOLANT OIL	RE EXHAUST	OIL PSI	POSIT			FLOW AC.H2O	BATTERY VOLTS	DUTY CYCLE	PERCENT OXYGEN		(LIARY F AOUSANDS		ENGINE HOURS
/17/96 12:07:35 UNIT 182							2 <del>4</del> 8	** 4	0.550	5 AC	: 77	555	1212
100 2195. 169.F 173.F 11/17/96 13:00:00 UNIT 182	927.F	53.	-2.3	16.3	125.	9,	13.4	55.0		2.45	133	269	1515.
90 2202. 168.F 173.F 177/96 14:00:00 UNIT 182	928.F	53.	-2,3	16.3	125.	ē. -	13.4	53.7	0.593	2.43	133	420	1515.
100 2209. 168.F 172.F ➡/17/96 15:00:00 UNIT 182	927.F	53.	-2.3	16.3	125.	8.	13.5	54.5	0.571	2.44	133	549	1516.
pe 2207. 167.F 171.F 11/17/96 16:00:00 UNIT 182	925.F	53.	-2.3	16.2	125.	7.	13.4	55.0	0.590	2.44	133	718	1517.
11/1/1/10 1010VIVV OR11 101	*	d=		:: =	शतह		:- ;	31.1	. 24:	ח זיי	:		17/5

11/17/96 17:00:00 UNIT 182	925.F	53.	-2.3	16.1	125.	9,	13.4	55.0	0 <b>.</b> 590	2.44	134	16	1519.
/17/96 18:00:00 UNIT 182	926.F	53.	-2.3	16.1	124.	9 <b>,</b>	13.4	54.6	0.591	2,42	134	165	1520.
17/96 18:15:40 UNIT 182												•	
Me 2199. 167.F 170.F 11/17/96 19:00:00 UNIT 182	926.F	53.	-2.3	16.1	124.	7.	13.5	53.6	0.592	2,42	134	203	i52i.
190 2207, 166.F 170.F 170.F 166.F 170.F	925.F	53,	-2,3	16.1	124.	9.	13.5	55.5	0.589	2.42	134	313	1521.
e 2204. 167.F 169.F	925.F	53.	-2.3	16.1	124.	<b>7.</b>	13.4	53.6	0.593	2.41	134	461	1522.
167.F 169.F	925.F	<b>5</b> 3.	-2.3	16.1	124.	9.	13.5	54.3	0.591	2.41	134	<b>4</b> 08	1523.
/17/96 22:00:00 UNIT 182 100 2196. 167.F 170.F	926.F	53.	-2.3	16.1	124.	9.	13.4	53.5	0.393	2.41	134	755	1524.
44/17/96 23:00:00 UNIT 182 60 2195. 166.F 169.F 1/15/96 00:00:00 UNIT 182	926.F	53.	-2,3	16.1	124.	9.	13.5	54.3	0.591	2.42	134	903	1525.
iệe 2198. 166.F 169.F	926.F	53.	-2.3	16.1	124.	9.	13.4	54.3	0.571	2.41	135	51	1526.
/18/96 01:00:00 UNIT 182 0 2198. 167.F 169.F	925.F	53.	-2,3	16.1	124.	9.	13.5	53.7	0.593	2.41	135	198	1527.
11/18/94 02:00:00 UNIT 183	924.F	53.	-2.3	16.1	124.	7.	13.4	53.8	0.592	2.40	135	346	1528.
/18/96 03:00:00 UNIT 182	925.F	53.	-2.3	16.1	124.	Ÿ.	13.4	54.9	0.590	2.42	135	493	1529.
11/18/96 04:00:00 UNIT 181 0 2188. 167.F 170.F	926.F	53.	-2.3	16.0	123.	9.	13.5	52.6	0.575	2,42	135	641	1530.
100 2192. 167.F 170.F	925.F	53.	-2.3	16.0	124.	9.	13.4	54.8	0.590	2.41	135	788	1531.
/18/94 05:37:23 UNIT 181 0 2189. 167.F 170.F	926.F	53.	-2.3	16.0	124.	9.	13.5	52.6	0.595	2.42	135	685	1532.
11/18/96 06:00:00 UNIT 181 180 2175. 168.F 171.F	927.F	53.	-2.3	16.0	123.	9,	13.3	53.3	0.57I	2.43	133	734	.===
7/18/96 07:00:00 UNIT 181 0 2190. 167.F 170.F	720.5	53,		20.0		·•	10.0						
- <del>1200</del> 2270. 22721 22721							.5		cna	0.40	•		1534.
718796 <b>89:00:00</b> UMIT 181		٠.			rvā.			35.1		2,42	134	V.W	
100 2175. 188.8 178.8 44/18/96 10:00:00 UNIT 182	926.F	53.	-2.3	15.7	123.	7,	13.3	55.9	9.588	2.42	136	380	1535.
0 2:52. 169.F 174.F 1/18/96 11:00:00 UNIT 182	923.F	53.	-2.4	15.9	123.	7.	13.3	56.3	0.587	2.44	136	529	1536.
100 2146. 168.F 175.F	925.F	53.	-2.4	15.9	124.	Ŧ.	13.3	54.5	0.591	2.46	136	678	1537.
@ 2178. 170.F 177.F	922 <b>.</b> F	53.	-2.3	16.0	124.	8.	13.2	54.1	0.592	2.64	136	829	1538.
11/18/96 13:00:00 UNIT 182 170.F 178.F	921 <b>.</b> F	53.	-2.2	15.9	124.	8.	13.3	56.2	0.588	2.68	136	991	1539.
•													
•													
H D OVETENE THE		MAREL US	3 S/N 182	;									
► V.R.SYSTEMS INC.		PERMIT N		<del>!</del>									
ENGINE TEMPERATU	RE	GIL	POSIT	TONS	WELL	FLOW	BATTERY	DUTY	PERCENT	AUX I	LIARY F	JEL	ENGINE
RPM COOLANT OIL						AC.H2O	VOLTS	CYCLE	OXYGEN	CFM TH	DUSANDS	-UNITS	HOURE
/16/96 14:00:00 UNIT 182						_		<b></b> -					
160 2191. 170.F 180.F 11/18/96 14:27:46 UNIT 182		52.	-i.8		129.	<b>8.</b>	13.1		0.585	2.58	137	151	1540.
0 2192. 170.F 179.F 1/18/96 15:00:00 UNIT 182	940.F	52.	-i.ē	17.1	129.	8.	13.3		0.586	2.58	137	224	1541.
100 2198. 169.F 179.F	941.F	52.	-1.9	17 <b>.</b> 1	128.	7.	13.2	57.0	0.586	2.56	137	308	1541.
0 2198. 168.F 177.F	740.F	52.	-2.0	17.1	128.	6.	13.2	56.5	0.587	2.55	137	464	1542.
11/18/96 17:00:00 UNIT 182	oso -	=-		, <del>-</del> .		-		<del>-</del>	र इसक			145	: = ==

ean mens

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	00:00 UNIT 182 169.F 176.F	942.F	52.	-2.0	i7.i	128.	8.	13.2	58.3	0.583	2.53	137	773	1544.
/18/96 18:	22:07 UNIT 182 169.F 176.F	943.F	53.	-2.2	17.0	128.	8.	13.1	58.1	0.584	2.50	137	830	1545.
18/96 19:	00:00 UNIT 182													
	168.F 175.F 00:00 UNIT 182	939.F	52.	-2.2	16.9	128.	8.	13.3	55.9		2.49	137	926	1545.
	168.F 174.F 00:00 UNIT 182	941.F	52.	-2.3	15.9	128.	9.	13.3	56.1	0.588	2.51	138	79	1546.
<b>1</b> 00 2203.	168.F 174.F 00:00 UNIT 182	941.F	52.	-2.3	16.9	128.	7.	13.3	56.9	0.586	2,49	138	231	1547.
₽ê 22ê2.	168.F 174.F	941.F	52.	-2.3	16.9	125.	7.	13.4	56.1	ê.588	2.49	138	384	1548.
100 2197.	00:00 UNIT 162 168.F 174.F	941.F	52.	-2.3	16.9	127.	7.	13.4	56.5	0.587	2.49	138	536	1549.
	00:00 UNIT 182 167.F 173.F	942.F	52.	-2.3	16.9	127.	7.	13.3	54.7	0.591	2.48	138	688	1550.
<del>7</del> 1/19/96 01:	00:00 UNIT 182 167.F 172.F	942.F	52.	-2.3	16.9	127.	7.	13.3	54.5	0.591	2.47	138	840	1551.
/19/96 02:	00:00 UNIT 182	942.F	52.	-2.3	16.9	127.	7.	13.4	56.3	0.587	2.48	138	992	1552.
11/19/96 03:	167.F 173.F 00:00 UNIT 182													
/19/96 04:	167.F 173.F 00:00 UNIT 182	941.F	52.	-2.3	16.9	127.	6.	13.4		<b>0.</b> 587	2.49	137	144	1553.
	168.F 173.F 00:00 UNIT 182	941.F	52.	-2.3	16.9	127.	á.	13.3	54.4	0.591	2.49	139	296	1554.
9 2183.	168.F 175.F 33:23 UNIT 182	940.F	52.	-2.3	16.9	127.	7.	13.4	56.7	0.587	2.50	139	448	1555.
100 2189.	168.F 173.F	941.F	52.	-2.3	16.9	127.	7.	13.4	55.7	0.589	2.48	139	533	1556.
00 2187.	00:00 UNIT 182 168.F 173.F	942.F	52.	-2.3	16.9	127.	7.	13.3	55.1	0.590	2.50	139	600	1556.
	00:00 UNIT 182 167.F 172.F	942.F	52.	-2.3	16.9	127.	7.	13.3	55.8	9 <b>.</b> 588	2.48	139	752	1557.
	00:00 UNIT 182 168.F 174.F	942.F	52.	-2.3	16.9	127.	7.	13.3	56.3	0.587	2.50	139	904	1558.
11/19/96 09:	00:00 UNIT 182 169.F 175.F	677 E	52.	-2.3	16.8	127.	7.	13.2	57.0	0 <b>.</b> 586	2.50	140	56	1559.
/19/96 10:	00:00 UNIT 182								56.3	0.587	2.51	140	209	1560.
<u> </u> 1/19/96 10:	169.F 176.F 17:09 UNIT 182			-2.3	16.8	127.	7.	13.2						
00 2211.	168.F 177.F	943.F	52.	<del>-</del> 2.3	17.5	130.	7.	13.2	55.0	0.590	2.81	140	253	1561.
<b>1</b> 0 2213.	00:00 UNIT 182 169.F 177.F	941.F	52.	-1.7	17.2	129.	á.	13.1	58.1	0.584	2.78	140	373	1561.
	170.F 178.F	943.F	52.	-2.7	17.4	129.	<b>6.</b>	13.2	58.4	0.583	2.60	140	534	1562.
	00:00 UNIT 182 169.F 178.F	948.F	52.	-2.7	17.8	131.	6.	13.1	58.6	0.583	2.62	140	693	1563.
-														
V.R.SYS	TEMS INC.		MODEL VI PERMIT N	3 5/N 183	2									
					FTAND	we i	TI AU	DATTERV	DUTY	PERCENT	ALIV 1	LIARY F	IE1	ENGINE
EMBINE RPM	TEMPERATU COOLANT OIL			POSI CARE.				BATTERY VOLTE		DEAGER				
1/19/94 13:	:02:53 UNIT 182													
100 2203.	169.F 179.F	946.F	52.	-2.7	17.8	131.	6.	13.1	58.5	0.583	2.62	140	700	1563.
00 2203.	00:00 UNIT 182 170.F 179.F	974.F	52.	-1.9	18.2	133.	5.	13.2	58.0	0.584	2.62	140	853	1564.

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11/19/96 15:00:00 UNIT 182

	ENGINE TEMPERATU	RE	OIL	P0817	TONE	WELL	FLOW	BATTERY	DUTY	PERCENT		LIARY F		ENGINE
	V.R.SYSTEMS INC.		MODEL V3 PERMIT N	5/N 182 O.	)									
	æ 2176. 171.F 181.F	947.F	52.	-4.7	17.8	133.	5.	13.0	58.2	0.584	2.64	143	972	1584.
	700 2170. 170.F 180.F 11/20/96 10:00:00 UNIT 182	945.F	53.	-4.7	17.8	131.	5.	13.2	57.3	0.585	2.57	143	814	1583.
	00 2166. 167.F 179.F //20/96 09:00:00 UNIT 182	947 <b>.</b> F	52.	-4.7	17.8	131.	6.	13.2	59.0		2.58	143	740	1583.
	11/20/96 08:31:39 UNIT 182										7 <del></del>	14.1	7.8 <del>¥</del>	ine.
	100 2171. 170.F 179.F	947 <b>.</b> F	52.	-4.0	17.5	131.	<u> </u>	15.1			- 27			
	00 2184. 169.F 179.F 11/20/96 08:30:50 UNIT 182	948.F	52.	-4.0	17.9	131.	6.	13.2	57.5	0.585	2.56	143	657	1582.
	Tee 2189. 149.F 178.F 11/20/96 08:00:00 UNIT 182	950.F	53.	-4.3	17.8	131.	5.	13.3	58.5	0.583	2.56	143	586	1581.
	00 2195. 169.F 177.F 1/20/96 07:00:00 UNIT 182	954.F	52.	-1.8	18.0	132.	5.	13.2	56.2	0.588	2.57	143	344	1580.
	11/20/96 06:00:00 UNIT 181								_			,	_,-	,
	1													
	1/20/96 05:43:42 UNIT 182 100 2211. 168.F 175.F	981 <b>.</b> F	53.	-1.3	18.1	133.	<u> </u>	13.4	56.0	0.588	2.58	143	301	1580.
	11/20/95 05:00:00 UNIT 182 100 2206. 159.F 177.F	957 <b>.</b> F	53.	-2.0	18.1	133.	5.	13.2	55.4	0.589	2.58	143	185	1579.
	1/20/96 04:00:00 UNIT 182 PO 2196. 170.F 178.F	952.F	52.	-2.3	17.9	133.	5.	13.3	56.2	0.588	2.60	143	27	1578.
1	1/20/96 03:00:00 UNIT 182 100 2171. 169.F 176.F	943.F	52.	-2.9	17.3	128.	5.	13.3	57.1	0.586	2.52	142	872	1577.
	11/20/96 02:00:00 UNIT 182 0 2166. 168.F 175.F	944.F	53.	-3.3	17.3	128.	5.	13.3	57.0	0.586	2.48	142	718	1576.
	1/20/96 01:00:00 UNIT 182 100 2158. 169.F 175.F	746.F	52.	<b>-</b> 3.1	17.3	128.	5.	13.2	55.7	0.589	2.49	142	565	1575.
É	11/20/96 00:00:00 UNIT 182 90 2181. 168.F 174.F	945.F	53.	-2.8	17.3	128.	5.	13.2	55.5	0.589	2.53	142	412	1574.
i,	/19/96 23:00:00 UNIT 182 16 2187. 168.F 174.F	944.F	53.	-2.á	17.3	128.	5.	13.4	57.9	0.584	2.50	142	259	1573.
	71/19/96 22:00:00 UNIT 182 190 2207. 168.F 174.F	951.F	53.	-2.0	17.7	130.	5.	13.3	55.3	0.589	2.54	142	105	1572.
	1/19/96 21:00:00 UNIT 182 10 2195. 168.F 175.F	951.F	53.	-2.4	17.7	130.	5.	13.4	55.3	0.587	2.55	141	950	1571.
- 3	1/19/96 20:00:00 UNIT 182 100 2197. 168.F 175.F	952.F	53.	-2.7	17.7	130.	5.	i3.3	56.5	<b>0.5</b> 87	2.55	141	795	1570.
•	11/19/96 19:00:00 UNIT 182 00 2198. 168.F 175.F	952.F	52.	-2.6	17.8	131.	5.	13.3	55.6	0.589	2.55	141	640	1569.
	1/19/96 18:00:00 18417 181 160 3:50 160.F 176.F	753.8	53.	-2.i	17.8	:3ē.	ė.	i3.i	57.2	<b>9.58</b> 6	2.57	141	463	1568.
	11/19/96 17:50:02 UNIT 182 100 2194. 168.F 176.F	952.F	53.	-2.6	17.8	131.	5.	13.2	56.5	0.587	2.57	141	457	1568.
	1/19/96 17:49:55 UNIT 182 00 2199. 169.F 175.F	952.F	52.	-2.5	17.8	131.	5.	13.3	55.2	0.590	2.57	141	457	1568.
:	1/19/96 17:00:00 UNIT 182 100 2203. 168.F 176.F	952.F	53.	-2.8	17.8	132.	an.	13.3	58.4	0.583	2.57	141	327	1567.
	00 2200. 169.F 178.F	953.F	52.	-2.6	17.9	133.	ē.	13.3	59.1	0.582	2.59	141	170	1566.
4	11/19/96 16:00:00 UNIT 182													

ENGINE TEMPERATURE OIL POSITIONS WELL FLOW BATTERY DUTY PERCENT AUXILIARY FUEL ENGINE RPM COOLANT OIL EXHAUST PSI CARB. BYPASS CFM-VAC.H20 VOLTS CYCLE OXYGEN CFM THOUSANDS-UNITS HOURS

1/20/96 10:45:18 UNIT 182
100 2266. 174.F 185.F 981.F 52. 0.1 19.7 146. 4. 13.1 58.5 0.583 2.86 144 98 1585.

100 2274. 174.F 185.F	982.F	52.	0.2	20.2	144.	2.	13.1	58.6	0.583	2.85	144	127	1585.
/20/96 10:57:58 UNIT 182 90 2235. 174.F 185.F	970.F	52.	-i.5	19.4	142.	<b>2.</b>	13.0	56 <b>.6</b>	0.587	2.30	144	134	1585.
<b>*</b>											5786 B	1 p	'n
											13/2	, (**) (**) (**)	•
•													
//20/76 11:00:00 UNIT 182	5/5 5	52.	-0.6	i8.7	137.	<b>3.</b>	12.9	57.0	0.586	2.93	144	140	1565.
T00 2224. 173.F 184.F 11/20/96 12:00:00 UNIT 182	962.F 949.F	52.	-5.2	17.7	133.	4.	12.9	61.6	0.577	2.92	144	316	(4) // (5) 102+
% 2200. 177.F 187.F 2/20/96 12:51:25 UNIT 182						4,	13.0	60.4	0.57 <del>9</del>	2.89	144	466	o Ired
100 2205. 176.F 187.F	957 <b>.</b> F	52.	-5.3	17.6	134.	<b>4</b> .	13.0	00.7	0.3/7	2:07	<u> </u>	TUU	1587.
•													
/20/96 13:00:00 UNIT 182													
11/20/96 14:00:00 UNIT 182	957.F	52.	-5.3	17.9	135.	4.	12.9		0.577	2,86	144	491	1587.
00 2197. 177.F 187.F 1/20/96 15:00:00 UNIT 182	957.F	52.	-5.3	18.5	135.	4.	12.9		0.57B	2.87	144	666	1588.
100 2197. 176.F 188.F	954.F	52.	-5.3	18.2	133.	<u>å</u> ,	12.9	62.2	<b>0.</b> 576	2.86	144	839	1587.
0 2205. 170.F 181.F 11/20/96 17:00:00 UNIT 182	955.F	52.	-5.2	18.2	133.	4:	13.0	60.9	0.578	2.85	145	11	1590.
100 2196. 170.F 180.F 20/96 17:26:17 UNIT 182	956.F	52.	-3.2	17.9	132.	4.	13.2	59.6	0.581	2.80	145	181	1591.
	956.F	53.	-5.0	17.5	131.	4.	13.1	58.9	0.582	2.78	145	255	1592.
0 2207. 169.F 179.F /20/96 19:00:00 UNIT 182	954.F	52.	-4.8	17.9	132.	4.	13.2	58.3	0.583	2.79	145	350	1592.
100 2184. 168.F 178.F 11/20/96 20:00:00 UNIT 182	956.F	52.	-4.8	17.9	i3i <b>.</b>	<b>4.</b>	13.2	58.3	ø.583	2.79	145	518	1593.
e 2194. 168.F 178.F	955.F	52.	-4.1	17.9	i3i.	<del>4</del> .	13.3	55.5	0.582	2.77	145	<del>5</del> 86	1594.
11/20/96 21:00:00 UNIT 182 100 2198. 169.F 178.F	954.F	52.	-4.2	17.8	131.	4.	13.2	56.8	0.586	2.76	145	853	1595.
/20/96 22:00:00 UNIT 182 6 2192. 169.F 176.F	956.F	52.	-5.0	17.8	i3i <b>.</b>	4.	i3.3	58.1	0.584	2.75	146	20	1594.
11/20/96 23:00:00 UNIT 182	955.F	52.	-4.5	iá.á	131.	4.	13.4	58.2	0.584	2.75	146	187	1597.
/21/96 00:00:00 UNIT 182 100 2215. 169.F 177.F	956.F	52.	-2.1	16.6	130.	4.	13.3	56.0	0.588	2.78	146	353	1598.
11/21/96 01:00:00 UNIT 182 00 2200. 168.F 176.F	951.F	52.	-0.4	17.0	127.	÷.	13.4	57.0					··.
<b>4.</b> /21/96 02:00:00 EMIT E1 100 25-						·· ,	•	em. 9	9 <u>5</u> 00	7.40	144	<u> </u>	1600°.

1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.:. 75.5 950.5			17.0	129.	4,	13.4	:A.A	0.587	2.71	146	854	1601.
	74.F 995.F	53.	-3.5	i7.i	129.	ā.	13.3	55.5	0.587	2.71	147	19	1602.
	74.F 954.F	52.	-3.4	17.i	129.	<del>4</del> .	i <b>3.</b> 3	55.2	<b>0.590</b>	2.73	147	185	1603.
1/21/96 06:00:00 UNIT 100 2206. 168.F 1	162 75.F 953.F	53.	-2.8	17.1	130.	5.	13.4	56.4	0.587	2.72	147	349	1604.
	76.F 951.F	52.	-3.4	17.0	130.	5.	13.3	54.8	0.590	2.71	147	514	1605.
100 2197. 169.F i	182 77.F 950.F	52.	-3.5	17.9	130.	<b>6.</b>	13.5	56.8	0.586	2.71	147	679	1606.
	182 76.F 950.F	53.	-3.6	17.1	129.	6.	13.5	55.1	0.590	2.70	147	842	1607.

V.R.SYSTEMS INC.

MODEL V3 S/N 182 PERMIT NO.

ENGINE RPM	TE? COOLANT	∜PERATU OIL	RE EXHAUST	OIL PSI	POSI1		WELL CFM-VA		BATTERY VOLTS	DUTY CYCLE	PERCENT OXYGEN		LIARY FL DUSANDS-		ENGINE HOURS
11/21/94 10: 400 2169. 1/21/96 10:	169.F	176.F	95i.F	52.	-3.8	17.1	129.	6.	13.5	56.3	<b>0.</b> 587	2.71	148	4	1608.
100 2186.	169.F	177 <b>.</b> F	949.F	52.	-3.8	17.0	130.	5,	13.6	57.4	Ø <b>.</b> 585	2.69	148	140	1609.
11/21/96 10: 198 2186.	166.F		967 <b>.</b> F	53.	-3.8	17.0	130.	2.	13.5	58.0	0.584	2.68	148	164	1607.
100 2175.	169.F	175.F	972.F	53.	-4.3	17.0	130.	2.	13.4	57.3	0.585	2.66	148	170	1609.
1/21/96 11 00 1984. 11/21/96 11	167.F	172.F	961.F	53.	-5.1	13.4	113.	3.	13.5	60.0	0.580	2.57	148	180	1609.
<u> 100 1931.</u>	167.F		952.F	53.	-4.9	12.4	107.	₹.	13.3	57.7	0.585	2.48	148	181	1607.
1/21/96 11 100 1830. 11/21/96 11	167.F	171.F	932.F	53.	-5.0	10.6	101.	<u> </u>	13.5	60 <b>.</b> 3	0.579	2.28	148	182	1609.
00 1748. 1/21/96 11	167.F	171.F	915.F	53.	-4.9	8.8	95.	4.	13.5	58.7	0.583	2.13	148	182	1607.
100 1701.	165.F	168.F	862.F	53.	-i.5	9.7	84.	Ą.	13.5	56.2	0.588	1.93	148	186	1607.
/21/96 11: 0 1772. 11/21/96 11:	165.F	167.F	854.F	53.	9.5	6.2	45.	5.	13.5	54.2	0.592	2.01	148	189	1610.
100 1864.	166.F	166.F	867.F	53.	14.0	2.9	32.	5.	13.5	56.4	0.587	2.13	148	192	1610.
/21/96 11: 40 18:8.	167.F	166.F	956.F	53.	18.2	-0.3	<b>⊕</b> .	á.	13.6	46.8	0.602	0.00	148	198	ići@.
11/21/96 11:	166.F	166.F	846.F	53.	22.7	-0.3	0.	6.	13.5	9.8	0.680	0.00	148	198	1610.
/21/96 11: 100 1587. _11/21/96 11:	166.F	165.F	870.F	53.	19.7	-0.3	0.	6.	13.5	9.8	0.680	0.00	148	198	1610.
#0 1552.	166.F	ićć.F	849.F	53.	19.4	-0.3	ê.	á.	13.6	9.8	0 <b>.6</b> 80	0 <b>.0</b> 0	148	198	1610.
11/21/96 11: 100 1507.	164.F	iái.F	739.F	53.	18.4	-0.4	<b>0.</b>	7.	13.6	9.8	0.680	9.00	148	199	1610.
1/21/96 11 ## 1536.		IT 182 162.F	738.F	53.	18.4	-0.4	0.	7.	13.5	9.8	0.680	0.00	148	199	1610.

11/21/96 11:37:33 LIMIT 414 ENG TMR OVRNG ENGINE FAILED ALARM UNIT 182

APPENDIX C
SYSTEM CHECKLIST

Checklist for System Shakedown

Site: CLL AFTS

Date: 11/11/96

Operator's Initials:

Fanimment	Check if OK	Comments
mandah	CIRCIN II OIN	COLIMICALICS
Liquid Ring Pump		
Aqueous Effluent Transfer Pump		
Oil/Water Separator	\	
Vapor Flow Meter		
Fuel Flow Meter	\ \ \	
Water Flow Meter		
Emergency Shut Off float Switch Effluent Transfer Tank		
Analytical Field Instrumentation GasTechtor O <sub>2</sub> /CO <sub>2</sub> Analyzer	)	
TraceTechtor Hydrocarbon Analyzer Oil/Water Interface Probe	7 7	
Magnehelic Boards	>	
Thermocouple Thermometer	7	

### $\label{eq:appendix} \textbf{D}$ D D ATA SHEETS FROM THE SHORT-TERM PILOT TEST

Revision 1 Page: 47 of 86 November 29, 1994 DRAFT

### Baildown Test Record Sheet

Site: KELLY AFB	
Well Identification: 008	
Well Diameter (OD/ID):	
Date at Start of Test: Nov 11, 96	Sampler's Initials:
Time at Start of Test: 1545	

# Initial Readings

Depth to	Depth to LNAPL (ft)	LNAPL	Total Volume
Groundwater (ft)		Thickness (ft)	Bailed (L)
16.45	15.55	.90	2.825

# Test Data

[ <del></del>			·
Sample Collection Time	Depth to Groundwater (ft)	Depth to LNAPL (ft)	LNAPL Thickness (ft)
1545	15.83	15.76	07
1545.5	15,83	15.74	.09
1546	15,83	15.74	.09
1546.5	15.84 -	15-74	- 10
1547	15.84	15.74	.10
15-48	15.85	15.74	- 1)
1549.	15.85	15.74	. ! ]
1550	15.85	15.75	.10
1555.	15.88	15.74	. 14
1615	15,92	15.73	. 19
1655	15.97	15.73	. 24
1726	15.47	15.73	. 24

0751 (11/12) 16.37 15.62 .75
Figure 9. Typical Baildown Test Record Sheet

Revision 1 Page: 47 of 86 November 29, 1994

DRAFT

# Baildown Test Record Sheet

Site: KELLY AFB	
Well Identification: 009	•
Well Diameter (OD/ID): 4:5	*****
Date at Start of Test: Nov 11, 96	Sampler's Initials:
Time at Start of Test: 16 4 8	

# Initial Readings

Depth to	Depth to LNAPL	LNAPL	Total Volume
Groundwater (ft)	(ft)	Thickness (ft)	Bailed (L)
18.29	16.92	1.37	6-7

# Test Data

Sample Collection Time	Depth to Groundwater (ft)	Depth to LNAPL (ft)	LNAPL Thickness (ft)
1648	17.28	17.20	08
1648.5	17.30	17.20	.10
1649	17.33	17.20	. 13
1649.5	17.33	17.20	. 13
1650	17.34	17.20	- 14
1650.5	17.34	17.20	-14
1651	17.35	17.20	-15
1651.5	17.36	17.20	.16
1652	17.37	17.20	-17
1652.5	17.37	17.20	-17
1658	17.43	17.19	-24
1703	17.47	17.17	.30

Figure 9. Typical Baildown Test Record Sheet

Revision 1 Page: 47 of 86 November 29, 1994

DRAFT

# Baildown Test Record Sheet

Site: KELLY AFB	
Well Identification: Oil	
Well Diameter (OD/ID): 4:5	<del></del>
Date at Start of Test: Nov 11, 1996	Sampler's Initials:
Time at Start of Test: 15.04 h.s	

# Initial Readings

Depth to Groundwater (ft)	Depth to LNAPL (ft)	LNAPL Thickness (ft)	Total Volume Bailed (L)	
16.59	15.21	1.38 Ft	4.95	7.3

8 L

# Test Data

			<u> </u>
Sample Collection Time	Depth to Groundwater (ft)	Depth to LNAPL (ft)	LNAPL Thickness (ft)
1504	15.57	15.53	04
1504.5	15-61	15.53	.08
1505	15-64	15.52	-12
1505.5	15.65	15.51	-14
1506	15.68	15.50	.18
1506.5	15.69	15,49	٠٤٥
1507	15.72	15.48	.24
1507.5	15.73	15.46	-26
1508.	15.75	15.47	.28
1509	15.78	15,47	. 3 /
1510	15.79	15,47	.32
1511	15.80	15.47	•33

Figure 9. Typical Baildown Test Record Sheet

Revision 1 Page: 47 of 86 November 29, 1994 DRAFT

# Baildown Test Record Sheet

Site:	KELLY A	8			
Well	Identification:O_U	, contd			
Well	Diameter (OD/ID):		·		
Date :	at Start of Test:			Sampler's Initials:	
Time	at Start of Test:	,			
<u>Initial</u>	Readings	·			
	Depth to Groundwater (ft)	Depth to LNAPL (ft)	LNAPL Thickness (ft)	Total Volume Bailed (L)	

# Test Data

Sample Collection Time	Depth to Groundwater (ft)	Depth to LNAPL (ft)	LNAPL Thickness (ft)
1512	15.81	15.47	34
1513	15,83	15.46	. 37
1514	15-83	15.46	.37
1519	15.85	15.45	.40
1524	15.88	15.44	- 44
15-34	15,92	15.43	.49
1606	16.05	15.43	.62
1636	16.13	15.38	.75
1730	16.28	15,35	.93
1800	16.33	15.33	1.00
0753 (11/12)	16.63	15.25	1.38

Figure 9. Typical Baildown Test Record Sheet

Page 1 of 1

Site: Kelly AFB

Test Type: <u>Initial Skimmer Well MW-11</u>

Start Date and Time: <u>11/12/96</u> 1430

Operators: Coonfare and Serpa

Date/Time	Run Time	LNAPL Recovery (volume collected in time period)	Groundwater Recovery (volume collected in time period)
11/12/96 1530	1	sheen	130 gallons
11/12/96 1705	2.58	sheen	49.1
11/12/96 1820	3.83	sheen	90
11/12/96 2110	6.67	sheen	125
11/13/96 0730	17	sheen	210.6
11/13/96 1305	22.6	sheen	162.5
11/13/96 1640	26.2	sheen	297.2
11/13/96 1820	27.8	sheen	89.9
11/13/96 2215	31.8	sheen	448.5
11/14/96 0725	40.9	6.3	846.8
Total		6.3	2449.3
	_		

Page \_\_\_\_ of \_\_\_\_

Site: Kelly AFB

Test Type: Bioslurper Well MW-11

State Date and Time: <u>11/14/96</u> 1119

Operators: Coonfare/Serpa

Date/Time	Run Time	LNAPL Recovery (volume collected in time period)	Groundwater Recovery (volume collected in time period)
11/14/96 1147	0.47	System shutdown	
11/14/97 1338	0.47	Restart system	
11/14/96 1410	1	sheen	651.6
11/14/96 1600	2.83	6.1 458	
11/14/96 2045	7.58	7.4	1187
11/15/96 0740	18.5	15.7	2629
11/15/96 1315	24.1	9.0	1284
11/15/96 2015	31.1	9.4	1610
11/16/96 0740	42.5	14.0	2637
11/16/96 1345	48.5	7.5	1347
11/16/96 1930	54.3	7.0	1276
11/17/96 0740	66.6	13.7	2738
11/17/96 1400	72.8	5.6	1395
11/17/96 2015	79.1	9.1	1404.4
11/18/96 0740	90.5	10.8	2428.6
11/18/96 1400	96.8	System shutdown	
11/18/96 1533	96.8	Restart system	
11/18/96 1625	97.7	8.6	1624
11/18/96 2025	101.7	6.3 864	
11/19/96 0730	112.8	5.4	2277
11/19/96 1215	117.5	20.4	973
Total		156	26,783.6

Page	١	of	1
rage	•	OI	

Site: Kelly AFB

Test Type: Bioslurper Well MW-09

State Date and Time: <u>11/19/96</u> 1308

Operators: Coonfare/Serpa

Date/Time	Run Time	LNAPL Recovery (volume collected in time period)	Groundwater Recovery (volume collected in time period)
11/19/96 1500	1.9	2.2	424
11/19/96 1950	6.7	10.0	1125
11/20/96 0745	18.6	23.0	2646
11/20/96 1300	23.9	13.4	1147
Total		48.6	5342

	i i	1
Page	l of	: 1

Site: Kelly AFB

Test Type: Second Skimmer Well MW-11

State Date and Time: <u>11/20/96</u> 1445

Operators: Coonfare/Serpa

Date/Time	Run Time	LNAPL Recovery (volume collected in time period)	Groundwater Recovery (volume collected in time period)
11/20/96 1930	4.7	4.2	651
11/20/96 1245	22.0	15.1	2401
Total		19.3	3052

Bloslurping Pilot Test (Data Sheet 1) Well Characteristics

Site: KELLY AFR

Test Type (skimmer, bioslurper vacuum extraction, drawdown):

Depth to Groundwater:

Depth to Fuel:

Depth of Slurper Tube;

Dale at Start of Test:

Time at Start of Test:

۽ ا	Time at Start of Test:				٠.				Operator's Initials: CC	ils: CC
		Well ID: 608	80		Well ID: 009	60		Well ID: O !!	= =	
	Date/Time	LNAPL	Water	Pressure (In II,O)	LNAPL	Water Level	Pressure (In II,O)	LNAPL	Water	Pressure
<del>-</del> v	11/11/96	15.55	16,45		16.92	18.29		15.21	16.59	
	0560	15.62 16.37	16.37		16.93	18.37		15,20	15,25 16,63	
	11/14/46	to p-3	End of skinner	tost a	We 11 011	•		15.6	15.6 15.80	
	11/11/16	15.91	16.99		17,32	17.32 18.57	5/22014		7 7 6	
	11/19/96	End Shoper on	- on Well 011	011	17.32.	17.32. 18.55		i	16.20	
	76/02/11	End Slurping	1 m Well	009	17.51	17.80		15,70 16,70	16.70	
			•				,		'n	
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							•			:

Figure 11. Typical Record Sheets for Bioslurper Pilot Testing

### Bioslurping Pilot Test (Data Sheet 2) Pilot Test Pumping Data

Page 1 of 1

Size: KELLY AFB

Operators: COONFARE / SERPA

Test Type: INITIAL SKIMMER

Depth to Groundwater: 16,63 Depth to Fuel: 15,25

Start Date: 11/12/96

Start Time: 1430

Well ID: 011

Depth, of Tube: 15.6

			Vapor I	Extractio	ם					
Date/Time	Run Time	Stack Pressure (in. H <sub>2</sub> O)	Dr	rbon ums H <sub>2</sub> O)	Flowrate (scfm)	Pump Stack Temp (°C)	Pump Head Vacuum (in. Hg)	Vac	ion Well uum H <sub>2</sub> O)	Drop Tobe Vacuum (in. Hzo)
11/12/96	14-	.045	•		24	48.2	22			45
11/12/46	2 h- 35 m.h	.05		·	25	51.2	2.2			45
11/12/96	375				25	51.6	·Z. Z			45
11/12/46	6. h-	.05 -045 <del>-05</del>			242-5	52.1	21			443
11/13/14	174-	.03			19	52.9	- 27			42
11/13/16	22.7	.04			21	54.2	· 21			40
11/13/96	26.3	.095			33	137.1	24			>60
1640	27.9	-09			. 32	38,2	2.4	•		50
11/13/96	31.5	.08			31	38,-5	24.			55
2215	40.6	.07			29	39.4	23		·	5 z
0.5										
	`									
		<u> </u>								

Figure 11. Typical Record Sheets for Bioslurper Pilot Testing (Continued)

### Bloslurping Pflot Test (Data Sheet 2) Pflot Test Pumping Data

Page 1 of Z

Site: KELLY AFB

Operators: COONFARE / SERPA

Test Type: BIOSL URPER

Depth to Groundwater: 15.85 Depth to Fuel: 15.6

Start Date: 11/14/96

Start Time: 1119

Well ID: 0 11

Depth of Tube: 15.7

		•	Vapor Extractio	п				
Date/Time	Run Time	Stack Pressure (In. H <sub>2</sub> O)	Carbon Drums (in. H <sub>2</sub> O)	Flowrate (scfm)	Pump Stack Temp (°C)	Pump Head Vacuum (in. Hg)	Extraction Well Vacuum (in. H <sub>2</sub> O)	Orop Tobe Vaccom (in. Hg)
11/14/16	14-	. 18	·	50	31.9	26	19	.19
11/14/96	34-	. 18		50	33.6.	25.5	20.5	19,5
11/14/96	7.8	.165		44	27.3	25.5	21	19.5
11/15/96	18.7	.19		51	27.9	25.5	21	19
11/15/46	24.2	.20	\ /	51	30.7	- 25.5	21.5	19.5
11/15/46	31.3	. 1.85		50	28.5	· 25,5	22	19
11/16/46	42.7	. 185		5-0	128.5	25	22	19
11/16/96	48.7	. 205	X	5 <sup>-</sup> 2	33,4	25.15	2.2	19.5
11/16/146	54.5	.195	/\	51	29.3	25.5	2.2	19.5
1930	66.7	.20	/\	51	29.5	25.5	22	19
11/17/14	7.3	. 20		51	30.3	25.5	2.2	19
11/17/96	79.3	.195		5-1	26.9	25.5	2 ک	19
11/18/96	90.6	-19		51	27.5	25.5	22	19
11/18/16	97.7	.20	<b>/</b>	5-1	29.3	25.5	22.5	19

Figure 11. Typical Record Sheets for Bioslurper Pilot Testing (Continued)

#### Bloslurping Pilot Test (Data Sheet 2) Pilot Test Pumping Data

Page 2 of 2

Site: KELLY AFB

Operators: COONFARE /SERPA

Test Type: BIOSLURPER, Contd

Depth to Groundwater: 15.85 Depth to Fuel: 15.6

Sun Date: 11/14/96

San Time: \_ /119

Well ID: \_\_ 0 / / \_\_\_

Depth, of Tube: 15.7

			Vapor Extraction	a			·	
Date/Time	Run Time	Stack Pressure (in. H <sub>2</sub> O)	Carbon Drums (in. H <sub>2</sub> O)	Flowrate (scfm)	Pump Stack Temp (°C)	Pump Head Vacuum (in. Hg)	Extraction Well Vacuum (in. H <sub>2</sub> O)	Orop Tobe Vaccom (in. Hg)
11/18/96	101.7	. 20	<u> </u>	5-1	28.7	25.5	2 3	.19
11/14/46	112.7		·/	5-1	28.9	25.5	23	19
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Figure 11. Typical Record Sheets for Bioslurper Pilot Testing (Continued)

#### Bloslurping Pilot Test (Data Sheet 2) Pilot Test Pumping Data

Page 1 of 1

Site: KELLY AFB

Operators: CouNFARE SERPA

Test Type: BIOSLURPER

Depth to Groundwater: 18.55 Depth to Fuel: 17.32

Son Date: 11/19/96

Sram Time: 1308

Well ID: 009

Depth, of Tube: 17.8

			Vapor Extraction	1				
Date/Time	Run Time	Stack Pressure (in. H <sub>2</sub> O)	Carbon Drums (in. H <sub>i</sub> O)	Flowrate (scfm)	Pump Stack Temp (*C)	Pump Head Vacuum (in. Hg)	Extraction Well Vacuum (in. H <sub>2</sub> O)	Vacuum (:n. Hg)
11/12/26	1.9	.205	\ · · /	52	30.0	25.5	<u>5</u> -	.19
11/19/96	6.7	رح.	\ ·/	5 <sup>-</sup> Z	28.0	25.5	5-	19
11/20/46		. 2 2		5 3	28.5	25,5	5-	19
11/20/46	23.6	- Z 5		5-6	32,6	25.5	5	19
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Figure 11. Typical Record Sheets for Bioslurper Pilot Testing (Continued)

### Blosiurping Pilot Test (Data Sheet 2) Pilot Test Pumping Data

Page \_ i of \_ i

Site: KELLY AFB

Operators: COON FARE SERPA

Test Type: SECOND SKIMMER

Depth to Groundwater: 16.75 Depth to Fuel: 15.75

Start Date: 11/20/91

Son Time: 1445

Well ID: 011

Depth, of Tube: 16.5

			Vapor Extractio	п				
Date/Time	Run Time	Stack Pressure (In. H <sub>2</sub> O)	Carbon Drums (in. H <sub>2</sub> O)	Flowrate (scfm)	Pump Stack Temp (°C)	Pump Head Vacuum (in. Hg)	Extraction Well Vacuum (in. H <sub>2</sub> O)	Orop Tobe Vaccom (in. Hg)
11/20/96	4.7	, 20	\ · /	51.	35.0	25.5	\	16.5
11/21/46	22.1	. 21	\ ·/	52	36.4.	25.5	/	16.5
1243						· ••		
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Figure 11. Typical Record Sheets for Bioslurper Pilot Testing (Continued)

## APPENDIX E LABORATORY ANALYTICAL REPORTS

SAMPLE NAME: KLRPV-1 ID#: 9611209-01A

Filenland Date of Collegions 1/1/17/26				
	The state of the s	##\$\$TIALHY#J###################################		
Compound	Det. Limit (ppbv)	Amount (ppb)		
Freon 12	400	Not Detected		
Freon 114	400	Not Detected		
Chloromethane	400	Not Detected		
Vinyl Chloride	400	Not Detected		
Bromomethane	400	Not Detected		
Chloroethane	400	Not Detected		
Freon 11	400	Not Detected		
1,1-Dichloroethene	400	Not Detected		
Freon 113	400	Not Detected		
Methylene Chloride	400	Not Detected		
1,1-Dichloroethane	400	Not Detected		
cis-1,2-Dichloroethene	400	2600		
Chioroform	400	Not Detected		
1,1,1-Trichloroethane	400	Not Detected		
Carbon Tetrachloride	400	Not Detected		
Benzene	400	Not Detected		
1,2-Dichloroethane	400	Not Detected		
Trichloroethene	400	3200		
1,2-Dichloropropane	400	Not Detected		
cis-1,3-Dichloropropene	400	Not Detected		
Foluene	400	Not Detected		
rans-1,3-Dichloropropene	400	Not Detected		
1,1,2-Trichloroethane	400	Not Detected		
l'etrachloroethene	400	Not Detected		
Ethylene Dibromide	400	Not Detected		
Chlorobenzene	400	Not Detected		
Ethyl Benzene	400	Not Detected		
n,p-Xylene	400	Not Detected		
o-Xylene	400	Not Detected		
Styrene	400	Not Detected		
,1,2,2-Tetrachloroethane	400	Not Detected		
,3,5-Trimethylbenzene	400	Not Detected		
,2,4-Trimethylbenzene	400	3000		
,3-Dichlorobenzene	400	Not Detected		
,4-Dichlorobenzene	400	Not Detected		
hlorotoluene	400	Not Detected		
,2-Dichlorobenzene	400	Not Detected		
,2,4-Trichlorobenzene	400	Not Detected		
lexachlorobutadiene	400	Not Detected		

SAMPLE NAME: KLRPV-1 ID#: 9611209-01A

EPA METHOD TO-14 GC/MS Full Scan

Compound	Det. Limit (ppbv)	Amount (ppbv)
Propylene	1600	Not Detected
1,3-Butadiene	1600	Not Detected
Acetone	1600	Not Detected
Carbon Disuifide	1600	Not Detected
2-Propanol	1600	Not Detected
trans-1,2-Dichloroethene	1800	Not Detected
Vinyl Acetate	1600	Not Datected
Chloroprene	1600	Not Detected
2-Butanone (Methyl Ethyl Ketone)	1600	Not Detected
Hexane	1600	Not Detected
Tetrahydrofuran	1600	Not Detected
Cyclohexane	1 <del>6</del> 00	3200
1,4-Dioxane	1600	Not Detected
Bromodichloromethane	1600	Not Detected
4-Methyl-2-pentanone	1600	Not Detected
2-Hexanone	1600	Not Detected
Dibromochloromethane	1600	Not Detected
Bromoform	1600	Not Detected
4-Ethyltoluene	1600	Not Detected
Ethanol	1600	Not Detected
Methyl tert-Butyl Ether	1600	Not Detected
Heptane	1600	Not Detected
TPH*	4000	15000000

<sup>\*</sup>Total Petroleum Hydrocarbons (C2 + Hydrocarbons) Referenced to Jet Fuel (MW = 156).

### Container Type: Tedlar Bag

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表现的,我们就是一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个
大学,上面上面,一直看到一个一直,一直看到一个一直,一直看到一个一直,一直看到一个一直,一直看到一个一直,一直看到一个一点,一直看到一个一点,一直看到一个一点,
。一个时间,我们就是一个时间,我们就是一个时间,我们就是一个时间,我们就是一个时间,我们就是一个时间,我们就是一个时间,我们就是一个时间,这个时间,这个时间,他
Surrouates  Octaffuciolopiene  Toluene-da  4-Biomoffucionejizene  14-Biomoffucionejizene  14-Biomoffuc
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Q = Exceeds Quality Control limits.

SAMPLE NAME: KICEV-1 ID#: 9611209-02A

File Name: (15/65 mall file in the common of	91f3006	Jate of Collection 11/4/786 Pare of Analysis 17/30/98
Compound	Det. Limit (ppbv)	Amount (ppbv)
Freon 12	71	Not Detected
Freon 114	71	Not Detected
Chloromethane	71	Not Detected
Vinyl Chloride	<b>71</b>	Not Detected
Bromomethane	71	Not Detected
Chloroethane	71	Not Detected
Freon 11	71	Not Detected
1,1-Dichloroethene	71	Not Detected
Freon 113	71	Not Detected
Methylene Chloride	71	Not Detected
1,1-Dichloroethane	71	Not Detected
cis-1,2-Dichloroethene	71	Not Detected
Chloroform	71	Not Detected
1,1,1-Trichioroethane	71	Not Detected
Carbon Tetrachloride	71	Not Detected
Benzenc	71	Not Detected
1,2-Dichloroethane	71	Not Detected
Trichloroethene	71	Not Detected
1,2-Dichloropropane	71	Not Detected
cis-1,3-Dichloropropene	71	Not Detected
Toluene	71	Not Detected
trans-1,3-Dichloropropene	71	Not Detected
1,1,2-Trichloroethane	71	Not Detected
Tetrachloroethene	71	Not Detected
Ethylene Dibromide	71	Not Detected
Chiorobenzene	71	Not Detected
Ethyl Benzene	71	Not Detected
m,p-Xylene	71	Not Detected
o-Xylene	71	Not Detected
Styrene	71	Not Detected
1,1,2,2-Tetrachloroethane	71	Not Detected
1,3,5-Trimethylbenzene	71	Not Detected
1,2,4-Trimethylbenzene	71	130
1,3-Dichlorobenzene	71	Not Detected
1,4-Dichlorobenzene	71	Not Detected
Chlorotoluene	71	Not Detected
1,2-Dichlorobenzene	71	Not Detected
1,2,4-Trichlorobenzene	71	Not Detected
Hexachlorobutadiene	71	Not Detected

SAMPLE NAME: KICEV-I

ID#: 9611209-02A

### EPA METHOD TO-14 GC/MS Full Scan

Compound	Det. Limit (ppbv)	Amount (ppbv
Propylene	280	Not Detected
1,3-Butadiene	280	Not Detected
Acetone	280	Not Detected
Carbon Disultide	280	Not Detected
2-Propanol	280	Not Detected
rans-1,2-Dichloroethene	280	Not Detected
/inyl Acetate	280	Not Detected
Chioroprene	280	Not Detected
P-Butanone (Methyl Ethyl Ketone)	280	Not Detected
lexane	280	Not Detected
Tetrahydrofuran	280	Not Detected
Cyclohexane	280	Not Detected
,4-Dioxane	280	Not Detected
Bromodichloromethane	280	Not Detected
-Methyl-2-pentanone	280	Not Detected
-Hexanone	280	Not Detected
Dibromochloromethane	280	Not Detected
Bromoform	280	Not Detected
-Ethyltoluene	280	Not Detected
thanol	280	Not Detected
lethyl tert-Butyl Ether	280	Not Detected
leptane	280	Not Detected
PH*	710	760000

\*Total Petroleum Hydrocarbons (C2 + Hydrocarbons) Referenced to Jet Fuel (MW = 156).

### Container Type: Tedlar Bag

Surrognies	76 Recovery Wethod Limits  #10 ************************************
Corallugrotoluena	
I oluene da la	70,180
	70/130

SAMPLE NAME: KLRPV-2 ID#: 9611209-03A

TOUS RECORDS		Paterot Collection 1748/96 Caterot Analysis 173098
Compound	Det. Limit (ppbv)	Amount (ppbv)
Freon 12	710	Not Detected
Freon 114	710	Not Detected
Chloromethane	710	Not Detected
Vinyi Chloride	710	Not Detected
Bromomethane	710	Not Detected
Chloroethane	710	Not Detected
Freon 11	710	Not Detected
1,1-Dichloroethene	710	Not Detected
Freon 113	710	Not Detected
Methylene Chloride	710	Not Detected
1,1-Dichloroethane	710	Not Detected
cis-1,2-Dichloroethene	710	2900
Chloroform	710	Not Detected
1,1,1-Trichloroethane	710	Not Detected
Carbon Tetrachloride	710	Not Detected
Benzene	710	Not Detected
1,2-Dichloroethane	710	Not Detected
Trichioroethene	710	2700
1,2-Dichloropropane	710	Not Detected
cis-1,3-Dichloropropene	710	Not Detected
Toluene	710	Not Detected
trans-1,3-Dichloropropene	710	Not Detected
1,1,2-Trichloroethane	710	Not Detected
Tetrachloroethene	710	Not Detected
Ethylene Dibromide	710	Not Detected
Chlorobenzene	710	Not Detected
Ethyl Benzene	710	Not Detected
m,p-Xylene	710	Not Detected
o-Xylene	710	Not Detected
Styrene	710	Not Detected
1,1,2,2-Tetrachloroethane	710	Not Detected
1,3,5-Trimethylbenzene	710	Not Detected
1,2,4-Trimethylbenzene	710	5400
1,3-Dichlorobenzene	710	Not Detected
1,4-Dichlorobenzene	710	Not Detected
Chlorotoluene	710	Not Detected
1,2-Dichlorobenzene	710	Not Detected
1,2,4-Trichlorobenzene	710	Not Detected
Hexachlorobutadiene	710	Not Detected

SAMPLE NAME: KLRPV-2 ID#: 9611209-03A

EPA METHOD TO-14 GC/MS Full Scan

Compound	Det. Limit (ppbv)	Amount (ppb)
Propylene	2800	Not Detected
1,3-Butadiene	2800	Not Detected
Acetone	2800	Not Detected
Carbon Disulfide	2800	Not Detected
2-Propanol	2800	Not Detected
rans-1,2-Dichloroethene	2800	Not Detected
Viny! Acetate	2800	Not Detected
Chioroprene	2800	Not Detected
2-Butanone (Methyl Ethyl Ketone)	2800	Not Detected
Hexane	2800	Not Detected
Tetrahydrofuran	2800	Not Detected
Cyclohexane	2800	3900
I,4-Dioxane	2800	Not Detected
Bromodichloromethane	2800	Not Detected
-Methyl-2-pentanone	2800	Not Detected
-Hexanone	2800	Not Detected
Dibromochloromethane	2800	Not Detected
Bromoform	2800	Not Detected
-Ethyltoluene	2800	Not Detected
thanol	2800	Not Detected
Nethyl tert-Butyl Ether	2800	Not Detected
feptane	2800	2900
*PH*	7100	29000000

<sup>\*</sup>Total Petroleum Hydrocarbons (C2 + Hydrocarbons) Referenced to Jet Fuel (MW = 156).

### Container Type: Tedlar Bag

是一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个	vanon, artia
Surrogates  Screen Control of the Co	
Octavo Goldene	CHANGE OF
	A Property
ACTION AND ADDRESS OF THE PROPERTY OF THE PROP	in the same of
4B tomoruoro de presenta de la companya del companya del companya de la companya	144444
	1000

Q = Exceeds Quality Control limits.

SAMPLE NAME: KICEV-2

ID#: 9611209-04A

FIRE PARTY AND THE PARTY AND T	9//8008 183	Date of Collection = Unif (8/96 Date of Analysis: Ff/30/06
Compound	Det. Limit (ppbv)	Amount (ppbv)
Freon 12	92	Not Detected
Freon 114	92	Not Detected
Chloromethane	92	Not Detected
Vinyl Chloride	92	Not Detected
Bromomethane	92	Not Detected
Chloroethane	92	Not Detected
Freon 11	92	Not Detected
1,1-Dichloroethene	92	Not Detected
Freon 113	92	Not Detected
Methylene Chloride	92	Not Detected
1,1-Dichloroethane	92	Not Detected
cis-1,2-Dichloroethene	92	Not Detected
Chloroform	92	Not Detected
1,1,1-Trichloroethane	92	Not Detected
Carbon Tetrachloride	92	Not Detected
Benzene	92	Not Detected
1,2-Dichloroethane	92	Not Detected
Trichloroethene	92	Not Detected
1,2-Dichloropropane	92	Not Detected
cis-1,3-Dichloropropene	92	Not Detected
Toluene	92	Not Detected
trans-1,3-Dichloropropene	92	Not Detected
1,1,2-Trichloroethane	92	Not Detected
Tetrachloroethene	92	Not Detected
Ethylene Dibromide	92	Not Detected
Chlorobenzene	92	Not Detected
Ethyl Benzene	92	Not Detected
m,p-Xylene	92	Not Detected
o-Xylene	92	Not Detected
Styrene	92	Not Detected
1,1,2,2-Tetrachloroethane	92	Not Detected
1,3.5-Trimethylbenzene	92	Not Detected
1.2,4-Trimethylbenzene	92	340
1,3-Dichlorobenzene	92	Not Detected
1,4-Dichlorobenzene	92	Not Detected
Chlorotoluene	92	Not Detected
1,2-Dichlorobenzene	92	Not Detected
1,2,4-Trichlorobenzene	92	Not Detected
Hexachlorobutadione	92	Not Detected
	<del></del>	Not Defected

SAMPLE NAME: KICEV-2 ID#: 9611209-04A

EPA METHOD TO-14 GC/MS Full Scan

Compound	Det. Limit (ppbv)	Amount (ppb
Propylene	370	Not Detected
1,3-Butadiene	370	Not Detected
Acetone	370	Not Detected
Carbon Disulfide	370	Not Detected
2-Propanol	370	Not Detected
rans-1,2-Dichloroethene	370	Not Detected
/inyl Acetate	370	Not Detecte
Chloroprene	370	Nat Detected
-Butanone (Methyl Ethyl Ketone)	370	Not Detecte
lexane	370	Not Detecte
etrahydrofuran	370	Not Detected
Cyclohexan <del>e</del>	370	Not Detected
,4-Dioxane	370	Not Detected
romodichioromethane	370	Not Detected
-Methyl-2-pentanone	370	Not Detected
-Hexanone	370	Not Detected
Ibromochloromethane	370	Not Detected
romoform	370	Not Detected
-Ethyltoluene	370	Not Detected
thanol	370	Not Detected
ethyl tert-Butyl Ether	370	Not Detected
eptane	370	Not Detected
PH*	920	1600000

Container Type: Tedlar Bag

Surrogales  Gerafijoraroluene  Folleng Barrogales  103 103 103 103 103 103 103 103 103 103	••	
	Surrogates Octativoratoluene Toluene 38 4-Bromolykoropenzene	ZHecovery Methos Links (Methos Links) (Methos Links

SAMPLE NAME: KICE-SP-1

ID#: 9611209-05A

EleName		Dair of Collection 1111/18/96
DIE Eertor:	Allers programmes and the second seco	uate of Analysis 17/30/96 - Li
Compound	Det. Limit (ppbv)	Amount (ppbv)
Freon 12	87	
Freon 114	87	: Not Detected : Not Detected
Chloromethane	87	Not Detected
Vinyl Chloride	87	Not Detected
Bromomethane	87	Not Detected
Chloroethane	87	Not Detected
Freon 11	87	Not Detected
1,1-Dichloroethene	87	Not Detected
Freon 113	87	Not Detected
Methylene Chloride	87	Not Detected
1,1-Dichloroethane	87	Not Detected
cis-1,2-Dichloroethene	87	Not Detected
Chloroform	87	Not Detected
1,1,1-Trichloroethane	87	Not Detected
Carbon Tetrachloride	87	Not Detected
Benzene	87	Not Detected
1,2-Dichloroethane	87	Not Detected
Trichloroethene	87	Not Detected
1,2-Dichloropropane	87	Not Detected
cis-1,3-Dichloropropene	87	Not Detected
Toluene	87	Not Detected
trans-1,3-Dichloropropene	87	Not Detected
1,1,2-Trichloroethane	87	Not Detected
Tetrachloroethene	87	Not Detected
Ethylene Dibromide	87	Not Detected
Chlorobenzene	87	Not Detected
Ethyl Benzene	87	Not Detected
m,p-Xylene	87	100
o-Xylene	87	Not Detected
Styrene	87	Not Detected
1,1,2,2-Tetrachloroethane	87	Not Detected
1,3,5-Trimethylbenzene	87	Not Detected
1,2,4-Trimethylbenzene	87	350
1,3-Dichlorobenzene	87	Not Detected
1,4-Dichlorobenzene	87	Not Detected
Chiorotoluene	87	Not Detected
1,2-Dichlorobenzene	87	Not Detected
1,2,4-Trichlorobenzene	87	Not Detected
Hexachlorobutadiene	87	Not Detected

SAMPLE NAME: KICE-SP-1 ID#: 9611209-05A

## EPA METHOD TO-14 GC/MS Full Scan

Compound	Det. Limit (ppbv)	- Amount (ppb)
Propylene	350	Not Detected
1,3-Butadiene	350	Not Detected
Acetone	350	Not Detected
Carbon Disulfide	350	Not Detected
2-Propanol	350	Not Detected
rans-1,2-Dichloroethene	350	Not Detected
Vinyl Acetate	350	Not Detected
Chloroprene	350	Not Detected
2-Butanone (Methyl Ethyl Ketone)	350	Not Detected
Hexane	350	Not Detected
Tetrahydrofuran	350	Not Detected
Cyclohexane	350	Not Detected
,4-Dioxane	350	Not Detected
Bromodichloromethane	350	Not Detected
l-Methyl-2-pentanone	350	Not Detected
-Hexanone	350	Not Detected
)ibromochloromethane	350	Not Detected
romoform	350	Not Detected
-Ethyltoluene	350	Not Detected
thanol	350	Not Detected
fethyl tert-Butyl Ether	350	Not Detected
leptane	350	Not Detected
TPH*	870	770000

•

#### Container Type: Tedlar Bag

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Surrogales: Wethod Linits
THE PROPERTY OF THE PROPERTY O
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要要是一个大型,我们就是一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个
Toluene (B) (100)
多数是这种是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人
"一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个
李明是1986年11日,11日,11日,11日,11日,11日,11日,11日,11日,11日
ABromotluorodenzeng
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SAMPLE NAME: Lab Blank ID#: 9611209-06A

Compound	Det. Limit (ppbv)	Amount (ppbv
Freon 12	0.50	Not Detected
Freon 114	0.50	Not Detected
Chloromethane	0.50	Not Detected
/inyl Chloride	0.50	Not Detected
3romomethane	0.50	Not Detected
Chloroethane	0.50	Not Detected
Freon 11	0.50	Not Detected
,1-Dichloroethene	0,50	Not Detected
Freon 113	0.50	Not Detected
Methylene Chloride	0.50	Not Detected
,1-Dichloroethane	0.50	Not Detected
is-1,2-Dichloroethene	0.50	Not Detected
Chloroform	0.50	Not Detected
,1,1-Trichioroethane	0.50	Not Detected
Carbon Tetrachloride	0.50	Not Detected
Benzene	0.50	Not Detected
,2-Dichloroethane	0.50	Not Detected
richloroethene	. 0.50	Not Detected
,2-Dichloropropane	0.50	Not Detected
is-1,3-Dichloropropene	0.50	Not Detected
oluene	0.50	Not Detected
ans-1,3-Dichloropropene	0.50	Not Detected
,1,2-Trichloroethane	0.50	Not Detected
etrachloroethene	0.50	Not Detected
thylene Dibromide	0.50	Not Detected
hlorobenzene	0.50	Not Detected
thyl Benzene	0.50	Not Detected
n,p-Xylene	0.50	Not Detected
-Xylene	0.50	Not Detected
tyrene	0.50	Not Detected
1,2,2-Tetrachloroethane	0.50	Not Detected
3,5-Trimethylbenzene	0.50	Not Detected
2,4-Trimethylbenzene	0.50	Not Detected
3-Dichlorobenzene	0.50	Not Detected
4-Dichlorobenzene	0.50	Not Detected
hlorotoluene	0.50	Not Detected
2-Dichlorobenzene	0.50	Not Detected
2,4-Trichlorobenzene	0.50	Not Detected
exachlorobutadiene	0.50	Not Detected

SAMPLE NAME: Lab Blank

ID#: 9611209-06A

### EPA METHOD TO-14 GC/MS Full Scan

Compound	Det. Limit (ppbv)	Amount (ppbv
Propylene	2.0	Not Detected
1,3-Butadiene	2.0	Not Detected
Acetone	2.0	Not Detected
Carbon Disulfide	2.0	Not Detected
2-Propanol	2.0	Not Detected
rans-1,2-Dichloroethene	2.0	Not Detected
/inyl Acetate	2.0	Not Detected
Chloroprene	2.0	Not Detected
-Butanone (Methyl Ethyl Ketone)	2.0	Not Detected
lexane	2.0	Not Detected
etrahydrofuran	2.0	Not Detected
Cyclohexane	2.0	Not Detected
,4-Dioxane	2.0	Not Detected
Bromodichloromethane	2.0	Not Detected
-Methyl-2-pentanone	2.0	Not Detected
-Hexanone	2.0	Not Detected
Dibromochloromethane	2.0	Not Detected
Bromoform	2.0	Not Detected
-Ethyltoluene	2.0	Not Detected
thanol	2.0	Not Detected
Methyl tert-Butyl Ether	2.0	Not Detected
leptane	2.0	Not Detected
ſ₽H*	5.0	Not Detected

<sup>\*</sup>Total Petroleum Hydrocarbons (C2 ÷ Hydrocarbons) Referenced to Jet Fuel (MW = 156).

### Container Type: NA

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Sunogates Octanicosotutepiela Screenia (1997) Torigone 38 4-Broftfoffuoroperzene:
Walter State of the Control of the C
4-Homo Hanzane



Alpha Analytical, Inc.

255 Glendale Avenue, Suite 21 Sparks. Nevada 89431 (702) 355-1044 FAX: 702-355-0406

FAX: 702-355-0406 1-800-283-1183 e-mail: alpha@powernet.net http://www.powernet.net/~alpha 2505 Chandler Avenue, Suite 1 Las Vegas, Nevada 89120 (702) 498-3312 FAX: 702-736-7523 1-800-283-1183

#### ANALYTICAL REPORT

Battelle

505 King Ave

Columbus Ohio 43201

Job#:

Phone: (614) 424-6199

Attn: Chris Coonfare

Sampled: 11/17/96

Received: 11/20/96

Analyzed: 11/26/96

Matrix: [

] Soil

[ ] Water

[ X ] Other

Analysis Requested: BTEX - Benzene, Toluene, Xylenes, Ethylbenzene

Methodology:

BTEX - EPA Method 624/8240

#### Results:

Client ID/	Parameter	Concentration	Limit
Lab ID		mg/Kg	mg/Kg
K-LNAPL-1	Benzene	ND	500
/BMI112096-01	Toluene	ND	500
, 5	Ethylbenzene	ND	500
	Total Xylenes	ND	500

ND - Not Detected

Approved by:

Roger L. Scholl, Ph.D. Laboratory Director

\_ Date: ∠

: 12/2/96



Alpha Analytical, Inc.

255 Glendale Avenue, Suite 21 Sparks, Nevada 89431 (702) 355-1044

FAX: 702-355-0406 1-800-283-1183 e-mail: alpha@powernet.net http://www.powernet.net/~alpha

ANALYTICAL REPORT

2505 Chandler Avenue, Suite 1 Las Vegas, Nevada 89120 (702) 498-3312 FAX: 702-736-7523 1-800-283-1183

Battelle

505 King Ave

Columbus Ohio 43201

Job#:

Phone: (614) 424-6199

Attn: Chris Coonfare

Sampled: 11/17/96

Received: 11/20/96

Analyzed: 11/26/96

Matrix: [

1 Soil

[ X ] Water

] Waste

Analysis Requested: TPH - Total Petroleum Hydrocarbons-Purgeable

Overtiteted De Caseline

Quantitated As Gasoline

BTEX - Benzene, Toluene, Ethylbenzene, Xylenes

Methodology:

TPH - Modified 8015/DHS LUFT Manual/BLS-191

BTEX - Method 624/8240

#### Results:

Client ID/ Lab ID	Parameter	Concentration		ction mit
K-W-1 /BMI112096-02	TPH (Purgeable) Benzene Toluene Ethylbenzene Total Xylenes	3.5 ND ND ND ND	1.0 2.0 2.0 2.0 2.0	mg/L ug/L ug/L ug/L ug/L

ND - Not Detected

Approved by:

Roger L. Scholl, Ph.D. Laboratory Director

te: <u>12/2/96</u>

Billing Name	Billing Information:	nation:	Al Ses	Alpha Analytical, Inc. 255 Glendale Avenue, Suite 21	Inc.		Doge #	\ \ \ \	\		
Address	S		_	irks, Nevada 89431			aga	50			
City, Sta	City, State, Zip			one (702) 355-1044 (702) 355-0406		\ <u></u>	<b>⋖</b>	Analyses Required	uired		
Phone	Phone Number	Fax		(102) 003-0400		\\ \_			) ) :		
Client P	Vame	ntille	#.O.4	dot #		\(\frac{1}{2}\)					_
Address	ş	1-10 - 1-	PWS#	· DWR #			<u></u>	<u> </u>	<u> </u>	_	
City, St	City, State, Zip		Phone #	Fax#		// // / / / / / / / / / / / / / / / /	<u></u>		<u></u>	<u></u>	
Time	Date	Matrix* Office Use Sampled by	Report Attention // S	J. W. Con	Total and type of	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		<u></u>	<u></u>	<u></u>	_
Sampled	Sampled Sampled	Selow Below	Sample Description		containers /	<u>~</u>	<u> </u>	_	<u> </u>	<u> </u>	_
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		Signature	Print Name			Company	y		Date	Time	
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Helinda	Heijnquished by/							`	\		
Received by	ed by										
Reling	Relinquished by										
. Received by	ed by										_
NOTE: S	Samples an	NOTE: Samples are discarded 60 days after results are reported unless other a	s reported unless other arrangements	irrangements are made. Hazardous samples will be returned to client or disposed of at client expense.	is samples will	will be returned to	client or dispos	sed of at client	expense.	70	

Form No.	<b>V</b>		oM tanin tadmul to tranistri	N	1   tree godect	1-3 3 water									Date/Time Received by:	(Signature)	Date/Time Received by:	(Signature)	
HAIN OF CUSTODY RECORD	SAMPLE TYPE ( </td <td>/ / / / / / / / / / / / / / / / / / / /</td> <td>7</td> <td>876.4 7/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8</td> <td>7</td> <td>×</td> <td></td> <td></td> <td>11-</td> <td>5</td> <td></td> <td>,</td> <td></td> <td></td> <td>Signature)   Relinquished by: (Signature)</td> <td>:</td> <td>Relinquished by: (Signature)</td> <td></td> <td>boratory by: Date/Time Remarks</td>	/ / / / / / / / / / / / / / / / / / / /	7	876.4 7/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8	7	×			11-	5		,			Signature)   Relinquished by: (Signature)	:	Relinquished by: (Signature)		boratory by: Date/Time Remarks
Н	Project Title		l	SAMPLE I.D.	K-LNAPL-1	K- V-									Date/Time Received by: (Signature)	0091 742/11	Date/Time Received by:	(a) distribution	Date/Time Received for Laboratory by: (Signature)
Baffelle Columbus Laboratories			SAMPLERS: (Signature)	DATE TIME	11/17/96 1300 4-5	11/12/96 1545 44									Relinquished by: (Signature)	T	Relinquished by: (Signature)		Relinquished by: (Signature)

## WORK ORDER #: 9611209

Work Order Summary

CLIENT:

Ms. Amanda Bush

BILL TO: Same

Battelle Memorial Institute

505 King Avenue

Columbus, OH 43201-2693

PHONE:

614-424-4996

INVOICE #

FAX:

614-424-3667

P.O. # 91221

DATE RECEIVED:

11/20/96

PROJECT # G462201-30C0901 Kcfly AFB

DATE COMPLETED:

FRACTION#	NI A BATE	man com	RECEIPT
	NAME	<u>TEST</u>	<u>VACJPRES.</u>
01A	KLRPV-1	TO-14	0 "Hg
02A	KICEV-1	TO-14	1.5 "Hg
03A	KLRPV-2	TO-14	1.5 "Hg
04A	KICEV-2	TO-14	2.5 "Hg
05A	KICE-SP-1	TO-14	1.0 "Hg
06A	Lab Blank	TO-14	NA
			- ·

## PRELIMINARY

LAB NARRATIVE:
All samples were diluted due to high levels of non target compouds.

CERTIFIED BY:

Laboratory Director

DATE: 12-5-96

 $\label{eq:appendix} \textbf{APPENDIX} \ \textbf{F}$  SOIL GAS PERMEABILITY TEST RESULTS

BATTELLE	RECORD 8	SHEET FOR AIR PERMEABILITY TEST	R PERMEABIL	ITY TEST	DATE/TIME: 14, 96 / 1119
DISTANCE FROM VENT WELL (ft. & tenths)	0.01	0.01	0.01		SITE: KELLY AFB
T) (II)	PT. CODE	PT. CODE	PT. CODE	PT. CODE	RECORDED BY: COONFARE SERPA
TIME FROM START-UP	MPA Green S.S.	MPA Bloc 9.0 ft	MPA Red 12.5 ft		
(MIN.)	PRESSURE (IN H <sub>2</sub> O)	PRESSURE (IN $H_2O$ )	PRESSURE (IN H <sub>2</sub> O)	PRESSURE (IN H <sub>2</sub> O)	COMMENTS
0	کن.	20,	-50.		
-	.05	٠٥٠	٤٥٠.		
R	90.	٥٥.	20.		
لم	20,	٥٥,	20,		
7	20.	20.	ho.		
0	.065	90.	,055		
	.05	.03	.035		
13	40.	250,	20,		
15/	.055	520:	20,		
17	٥٥.	200.	50.		
27	. 20	.080.	.05		Shot down biostuper
139	١	1	1		24 Restant 3:05/2028
141	.50	.25	. 12		•
143	.055	.03	20.	·	

RECORD SHEET FOR AIR PERMEABILITY TEST DATE/TIME:	5.0 10.0 10.0 SITE: KELLY AFB	CODE PT. CODE PT. CODE RECORDED BY:	Green MPA Blue MPA Red	9.0 ft 12.5 ft	ESSURE PRESSURE PRESSURE PRESSURE (IN $H_2O$ ) (IN $H_2O$ ) (IN $H_2O$ ) (IN $H_2O$ )	o4 ,04 bo. 40	095 .11	41.	+ + +	13 . I L	Shotdown shoper on well	7. 7.					
RECORD SHEET FO	10.01	PT. CODE   PT. COI	MPA Green MPA BI	5.5 ft 9.0 f	PRESSURE PRESSU (IN H <sub>2</sub> C)	ho. ho.	.095	105	+	ri. 51.	]						
BATTELLE	DISTANCE FROM VENT WELL (ft. & tenths)		TIME	START-UP	(MIN.)	9821	2701	4341	2746	9869	1215 4-3 11/12/96	1308h-s 11/19/96	) 1.17.8				

BATTELLE	RECORD	SHEET FOR AL	SHEET FOR AIR PERMEABILITY TEST	ITY TEST	DATE/TIME N. 14 9/ /
DISTANCE FROM VENT WELL (ft. & tenths)	23.0	23.0	23.6		Y AFB
TIME	PT. CODE	PT. CODE	PT. CODE	PT. CODE	RECORDED BY: COMERNE / SERPA
FROM START-UP	MPB Green 6.0 ft	MPB B1.e 10.0 ft	MPB Red 13.5 ft.		
(MIN.)	PRESSURE (IN H <sub>2</sub> O)	PRESSURE (IN H <sub>2</sub> O)	1 7 -	PRESSURE (IN H,O)	COMMENTS
٥	0	٥	0		
	.025	20.	۲٥.		
3	,025	10,	.03		
ان	0	,0.	20.		
7	200.	.03	.03		
8	0	0	0,0		
-	٥	0	5 0		
13	ગ	10.	510		
15	0	10:	20.		
17	0	10.	.03		
. 22	)0.	۲0,	.03		+ 3>
13.4	þ	4	1		9
141	0	0	0		Nestart Didslurper
143	200.	٥	0		

DISTANCE FROM VENT WELL (ft. & tenths)	23.0	23.0	23. 0 23. 0 23. 0	117 1531	DATE/TIME: SITE: <u>Kely</u> Afb
TIME FROM START-UP	PT. CODE	MFB 81-e 10.0 f+	PT. CODE MPB Red /3.5 ft	PT. CODE	RECORDED BY:
	PRESSURE (IN H <sub>2</sub> O)	COMMENTS			
1286	1.10	.50	. 255		
2701	750	5,0	2.0		
4341	> 50	1.1	1.0		
5746	200	5,0	. 1.25		
9869	V 50	3.5	1.5		
12154-5 (11/19/96)	,	1			Shutdown biochase
1308 hrs (11/19/46)	1	1	1		i
1448	70	0	0		1

BATTELLE	RECORD	SHEET FOR A	SHEET FOR AIR PERMEABILITY TEST	ITY TEST	DATE/TIME: Nov 14 96 / 1119
DISTANCE FROM VENT WELL (ft. & tenths)	30.0	30.0	30.0		SITE: KELLY AFB
HWE	PT. CODE	PT. CODE	PT. CODE	PT. CODE	RECORDED BY: Coonfare/SERPA
FROM	MPC Green	>~18 WPC	MPC		
START-UP	tt 0.9	10.0 Ft	14.0 Ft		
(MIN.)	PRESSURE (IN $H_2O$ )	PRESSURE (IN H <sub>2</sub> O)	PRESSURE (IN H <sub>2</sub> O)	PRESSURE (IN H <sub>2</sub> O)	COMMENTS
೧	ဂ	0	0		
~	0	0	10.		
3	0	٥	10.		
5	10,	10.	10.		
٨	.01	10.	10.		
5	.005	300.	200.		
-	၁	0	.005		
7.	.015	10.	/0,		
اح ا	200.	10.	10.		
71	10.	.01	510.		
7.5	10.	10.	10,		Shot down hind
139	ļ				Restart hand
( 11 .	٥	0	0		ı
143	0	0	500.		

# APPENDIX G IN SITU RESPIRATION TEST RESULTS

			Recor	d Sheet for In Sit	Record Sheet for In Situ Respiration Test		
Site KELLY	y AFB			Monitoring Point	nt MPA Red	d 12.5	ナナ・
Shutdown Date	te 11/21/96	,		O <sub>2</sub> /CO <sub>2</sub> Meter No.	No.		TPH Meter No.
Shutdown Time	ne 1500	hrs		Recorded by	COUNTARE/SE.	SERFA	
Date	Time	O <sub>2</sub> (%)	CO, (%)	TPH (mqq)	He (%)	Temperature (°C)	Comments
11/21/96	1500	12	٥	93	0		
11/21/96	1530	21	0	091	٥		
11/21/16	1700	12	0.25	340		,	
11/21/96	0681	18.5	<i>ن</i> ، ۲	085			
11/21/96	2030	17,0	0.25	720			
11/21/96	2230	14.5	٠. د ح	1100	1		
76/22/11	0030	13.5	52.0	0801			
11/22/16	0330	11.5	0	1300	1		
11/22/96	0730	11.0	0.5	0091			
11/22/96	0001	5.6	0.25	018	1		194 7.7 1.1 / HAL
11/22/96	1300	7.5	٥, ح	1220	1		1.1 /
11/22/16	1530	7.0	٥.9	1200	-		1:1/5
11/22/16	1700	5,5	0.5	1600			1:1 / 4
						•	
				-			
	•	·					7

	5 ft	TPH Meter No.		Comments								TPH ~/ 1:1 4:12+01	1:1	3	1:1 /3	1:1	3				
	Red 13.		SERPA	Temperature (°C)			•														
Sheet for In Situ Respiration Test	MPB	No.	COONFARE /S	He (%)	0	0		•				-			_	-	-				
l Sheet for In Sit	Monitoring Point	O <sub>2</sub> /CO <sub>2</sub> Meter No.	Recorded by	TPH (ppm)	081	081	5 80	078	1400	1440	1440	140	1800	1620	1800	2000	1940				
Record				CO <sub>2</sub> (%)	0	0	0	0.25	1.0	0.25	52.0	0	0.25	٥. د ح	0.25	0.25	0.25	•			
		9	hrs	O <sub>2</sub> (%)	12	12	20,0	17.5	13,0	12.0	10.5	9.0	4.0	3.0	2.0	2.0	٠. ك. ١				
	X AFB	B 11/21/96	1500		1500	1530	0011	1830	2030	2230	0030	0330	0730	1000	1300	1530	1700				
	Site KELLY	Shutdown Date	Shutdown Time	Date	11/21/46	11/21/96	11/21/46	76/12/11	11/21/96	96/12/11	11/22/96	11/22/46	11/22/96	11/22/96	11/22/11	11/22/46	11/22/96				

			Record	d Sheet for In Sit	Record Sheet for In Situ Respiration Test		
Site KELLY	Y AFB			Monitoring Point MPC	nt MPC Red	0.41 P.	<i>+</i> \$ 0
Shutdown Date	11/21/46	9		O <sub>2</sub> /CO <sub>2</sub> Meter No.	No.		TPH Meter No.
Shutdown Time		4-5		Recorded by Coonfare,	COONFARE /SERPA	PA	
Date	Time	O <sub>2</sub> (%)	CO <sub>2</sub>	TPH (mqq)		Temperature (°C)	Comments
96/12/11	1500	12	0	048	0		
76/12/11	1530	12	0	200	0		
11/21/96	1700	20.5	0.25	500.	1	•	
96/12/11	1830	18.0	0.25	700	1		
11/21/96	2030	15.5	0.25	1180	1		
11/21/46	2230	12.5	0.25	1540	1		
11/22/46	0030	11.0	0.25	1400	)		
11/22/96	0330	10.5	0,25	0091	1		
11/25/46	0730	8.5	52.0	1280	1		TPH W/ 1:1 4:1-4:0
11/22/16	(000)	له . لم الم	0.25	1240	•		1:1
11/22/46	1300	7.0	٥. ٢	0991	١		1:1
11/22/96	1530	5.0	، ٥٠ ک	. 0 4 41			1:1 /3
11/22/46	1700	. ح. ح	0,25	0011	1		TP# ~/ 1:1 4:1-12
			-			-	
				·			
		_					
		·					